Lecture 10: LQ with Frequency Shaped Cost Function (FSLQ)

Background
Parseval's Theorem
Frequency-shaped LQ cost function
Transformation to a standard LQ

Big picture

why are we learning this:

▶ in standard LQ, Q and R are constant matrices in the cost function

$$J = \int_0^\infty \left(x^T(t) Q x(t) + \rho u^T(t) R u(t) \right) dt \tag{1}$$

 \blacktriangleright how can we introduce more design freedom for Q and R?

Connection between time and frequency domains

Theorem (Parseval's Theorem)

For a square integrable signal f(t) defined on $[0,\infty)$

$$\int_{0}^{\infty} f^{T}(t) f(t) dt = \frac{1}{2\pi} \int_{-\infty}^{\infty} F^{T}(-j\omega) F(j\omega) d\omega$$

1D case:

$$\int_{0}^{\infty} |f(t)|^{2} dt = \frac{1}{2\pi} \int_{-\infty}^{\infty} |F(j\omega)|^{2} d\omega$$

Intuition: energy in time-domain equals energy in frequency domain For the general case, f(t) can be acausal. We have

$$\int_{-\infty}^{\infty} f^{T}(t) f(t) dt = \frac{1}{2\pi} \int_{-\infty}^{\infty} F^{T}(-j\omega) F(j\omega) d\omega$$

Discrete-time version:

$$\sum_{k=-\infty}^{\infty} f^{T}(k) f(k) = \frac{1}{2\pi} \int_{-\infty}^{\infty} F^{T}(e^{-j\omega}) F(e^{j\omega}) d\omega$$

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History

Marc-Antoine Parseval (1755-1836):

- French mathematician
- published just five (but important) mathematical publications in total (source: Wikipedia.org)

Frequency-domain LQ cost function

From Parseval's Theorem, the LQ cost in frequency domain is

$$J = \int_0^\infty \left(x^T(t) Q x(t) + \rho u^T(t) R u(t) \right) dt$$
 (2)

$$= \frac{1}{2\pi} \int_{-\infty}^{\infty} \left(X^{T}(-j\omega) QX(j\omega) + \rho U^{T}(-j\omega) RU(j\omega) \right) d\omega \qquad (3)$$

Frequency-shaped LQ expands Q and R to frequency-dependent functions:

$$J = \frac{1}{2\pi} \int_{-\infty}^{\infty} \left(X^{T}(-j\omega) Q(j\omega) X(j\omega) + \rho U^{T}(-j\omega) R(j\omega) U(j\omega) \right) d\omega$$
(4)

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Frequency-domain LQ cost function

Let

$$Q(j\omega) = Q_f^T(-j\omega)Q_f(j\omega) \succeq 0, \ X_f(j\omega) = Q_f(j\omega)X(j\omega)$$

 $R(j\omega) = R_f^T(-j\omega)R_f(j\omega) \succ 0, \ U_f(j\omega) = R_f(j\omega)U(j\omega)$

(4) becomes

$$J = \frac{1}{2\pi} \int_{-\infty}^{\infty} \left(X_f^T(-j\omega) X_f(j\omega) + \rho U_f^T(-j\omega) U_f(j\omega) \right) d\omega$$

which is equivalent to (using Parseval's Theorem again)

$$J = \int_0^\infty \left(x_f^T(t) x_f(t) + \rho u_f^T(t) u_f(t) \right) dt$$
 (5)

Frequency-domain LQ cost function

Summarizing, we have:

plant:

$$\begin{cases} \dot{x}(t) = Ax(t) + Bu(t) \\ y(t) = Cx(t) \end{cases}$$
 (6)

new cost:

$$J = \int_0^\infty \left(x_f^T(t) x_f(t) + \rho u_f^T(t) u_f(t) \right) dt \tag{7}$$

filtered states and inputs:

$$x(t) \longrightarrow Q_f(s) \longrightarrow x_f(t), \quad u(t) \longrightarrow R_f(s) \longrightarrow u_f(t)$$

We just need to translate the problem to a standard one [which we know (very well) how to solve]

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Frequency-domain weighting filters

state filtering

$$x(t) \longrightarrow Q_f(s) \longrightarrow x_f(t)$$

- ▶ a MIMO process in general: if $x(t) \in \mathbb{R}^n$ and $x_f(t) \in \mathbb{R}^q$, then $Q_f(s)$ is a $q \times n$ transfer function matrix
- ▶ $Q_f(s)$: state filter; designer's choice; can be selected to meet the desired control action and the performance requirements
- write $Q_f(s) = C_1(sI A_1)^{-1}B_1 + D_1$ in the general state-space realization:

$$\begin{cases}
\dot{z}_1(t) = A_1 z_1(t) + B_1 x(t) \\
x_f(t) = C_1 z_1(t) + D_1 x(t)
\end{cases}$$
(8)

Frequency-domain weighting filters

input filtering

$$u(t) \longrightarrow R_f(s) \longrightarrow u_f(t)$$

- ▶ $R_f(s)$: input filter; designer's choice; can be selected to meet the robustness requirements
- write $R_f(s) = C_2(sI A_2)^{-1}B_2 + D_2$ in the general state-space realization:

$$\begin{cases} \dot{z}_2(t) = A_2 z_2(t) + B_2 u(t) \\ u_f(t) = C_2 z_2(t) + D_2 u(t) \end{cases}$$
(9)

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Back to time-domain design

Combining (6), (8) and (9) gives the enlarged system

$$\frac{d}{dt} \underbrace{\begin{bmatrix} x(t) \\ z_1(t) \\ z_2(t) \end{bmatrix}}_{x_e(t)} = \underbrace{\begin{bmatrix} A & 0 & 0 \\ B_1 & A_1 & 0 \\ 0 & 0 & A_2 \end{bmatrix}}_{A_e} \begin{bmatrix} x(t) \\ z_1(t) \\ z_2(t) \end{bmatrix} + \underbrace{\begin{bmatrix} B \\ 0 \\ B_2 \end{bmatrix}}_{B_e} u(t)$$

and

$$x_f(t) = \underbrace{\begin{bmatrix} D_1 & C_1 & 0 \end{bmatrix}}_{C_e} \begin{bmatrix} x(t) \\ z_1(t) \\ z_2(t) \end{bmatrix}$$
$$u_f(t) = \begin{bmatrix} 0 & 0 & C_2 \end{bmatrix} x_e(t) + D_2 u(t)$$

Summary of solution

With the enlarged system, the cost

$$J = \int_0^\infty \left(x_f^T(t) x_f(t) + \rho u_f^T(t) u_f(t) \right) dt$$
 (10)

translates to

$$J = \int_{0}^{\infty} \left(x_{e}^{T}(t) Q_{e} x_{e}(t) + 2u^{T}(t) \underbrace{\left[\begin{array}{ccc} 0 & 0 & \rho D_{2}^{T} C_{2} \end{array} \right]}_{N_{e}} x_{e}(t) + u^{T}(t) \underbrace{\rho D_{2}^{T} D_{2}}_{R_{e}} u(t) \right) dt$$

$$Q_{e} = \begin{bmatrix} D_{1}^{T} D_{1} & D_{1}^{T} C_{1} & 0 \\ C_{1}^{T} D_{1} & C_{1}^{T} C_{1} & 0 \\ 0 & 0 & \rho C_{2}^{T} C_{2} \end{bmatrix}$$

solution (see appendix for more details):

$$u(t) = -R_e^{-1}(B_e^T P_e + N_e)x_e(t) = -Kx(t) - K_1z_1(t) - K_2z_2(t)$$

algebraic Riccati equation:

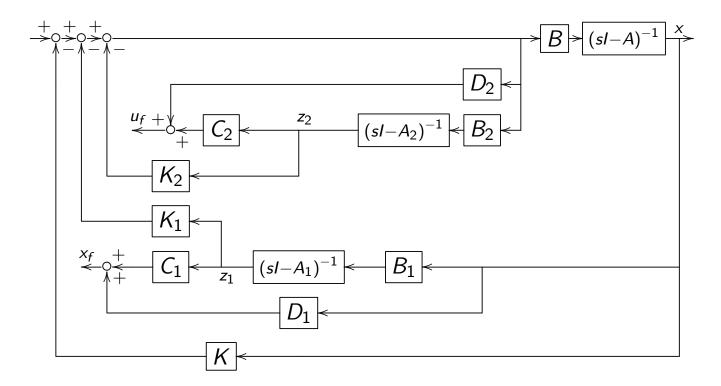
$$A_e^T P_e + P_e A_e - (B_e^T P_e + N_e)^T R_e^{-1} (B_e^T P_e + N_e) + Q_e = 0$$

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Implementation

structure of the FSLQ system:



Appendix: general LQ solution

Consider LQ problems with cost

$$J = \int_0^\infty \left(x^T(t) \underbrace{C^T C}_{Q} x(t) + 2u^T(t) Nx(t) + u^T(t) Ru(t) \right) dt \quad (11)$$

and system dynamics

$$\dot{x}(t) = Ax(t) + Bu(t)$$

- assume (A, B) is controllable/stabilizable and (A, C) is observable/detectable
- the solution of the problem is

$$u(t) = -R^{-1}(B^{T}P + N)x(t)$$

$$A^{T}P + PA - (B^{T}P + N)^{T}R^{-1}(B^{T}P + N) + Q = 0$$

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Appendix: general LQ solution

Intuition: under the assumptions, we know we can stabilize the system and drive x(t) to zero. Consider $V(t) = x^{T}(t)Px(t)$

$$V(\infty) = \int_0^\infty \dot{V}(t) dt$$

$$= \int_0^\infty \left(x^T(t) \left(PA + A^T P \right) x(t) + 2x^T(t) PBu(t) \right) dt$$

Adding (11) on both sides yields

$$V(\infty) - V(0) + J =$$

$$\int_{0}^{\infty} \left(x^{T}(t) \left(Q + PA + A^{T} P \right) x(t) + 2x^{T}(t) \left(PB + N^{T} \right) u(t) + u^{T}(t) Ru(t) \right) dt$$
(12)

▶ to minimize the cost, we are going to re-organize the terms in (12) into some "squared" terms

Appendix: general LQ solution

"completing the squares":

$$2x^{T}(t) (PB + N^{T}) u(t) + u^{T}(t) Ru(t) = \|R^{1/2} u(t) + R^{-1/2} (B^{T}P + N) x(t)\|_{2}^{2}$$
$$-x^{T}(t) (PB + N^{T}) R^{-1} (B^{T}P + N) x(t)$$

hence (12) is actually

$$V(\infty) - V(0) + J$$

$$= \int_{0}^{\infty} \left[x^{T}(t) \left(Q + PA + A^{T}P - \left(PB + N^{T} \right) R^{-1} \left(B^{T}P + N \right) \right) x(t) + \left\| R^{1/2}u(t) + R^{-1/2} \left(B^{T}P + N \right) x(t) \right\|_{2}^{2} \right] dt$$

hence $J_{\min} = V(0) = x^{T}(0) Px(0)$ is achieved when

$$Q + PA + A^{T}P - \left(PB + N^{T}\right)R^{-1}\left(B^{T}P + N\right) = 0$$
and $u(t) = -R^{-1}\left(B^{T}P + N\right)x(t)$

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