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Numerical Modeling of Extracorporeal Shock Wave Therapy with Finite Volume Methods

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# ESWT Background

- Similar treatment to Shock wave Lithotripsy (ESWL)
- Shock waves are used to treat musculoskeletal conditions
- Typical Treatment
  - 1000-4000 shocks
  - 1-4 shocks per second



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# ESWT Shock Wave Properties

# Shock Wave Generated by a spark plug source (electrohydraulic lithotripter)



#### Typical Wave Form

Shock waves in lithotripsy are weak and can be modeled as discontinuities.



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### ESWT - material heterogeneities

#### Numerical Representation of Lithotripter



Interfaces: Brass/Water, Air/Water, Water/Bone

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Bone data is extracted from CT scans and modeled with uniform material properties.





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## ESWT Shock Wave Propagation

Wave Propagation in Heterogeneous media



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### Finite volume method

#### Finite volume methods

Integral form of the conservation law,

$$\frac{\partial}{\partial t} \int_{x_{i-1/2}}^{x_{i+1/2}} q(x,t) \, dx = f(q(x_{i-1/2})) - f(q(x_{i+1/2}))$$

can be written in PDE form as  $q_t + f(q)_x = 0$  and used to define the numerical method.

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### Finite volume method

Integral form:  $\frac{\partial}{\partial t} \int_{x_{i-1/2}}^{x_{i+1/2}} q(x,t) \, dx = f(q(x_{i-1/2})) - f(q(x_{i+1/2}))$ 



Define:  $Q_i^n \approx \int_{x_{i-1/2}}^{x_{i+1/2}} q(x, t_n) dx$ Numerical method:  $Q_i^{n+1} = Q_i^n - \frac{\Delta t}{\Delta x} (F_{i+1/2} - F_{i-1/2})$ Numerical flux:  $F_{i-1/2} \approx \frac{1}{\Delta t} \int_{t_n}^{t_{n+1}} f(q(x_{i-1/2}, t)) dt$  Numerical Modeling of Extracorporeal Shock Wave Therapy with Finite Volume Methods

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### The Riemann problem

The Riemann problem for  $q_t + f(q)_x = 0$  has special initial data

$$q(x,0) = \begin{cases} q_l & \text{if } x < 0\\ q_r & \text{if } x > 0 \end{cases}$$

Solutions to this problem are used to define the numerical fluxes which update cell averages.

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The Linear Acoustics Equations with spatially varying material parameters are:

$$\begin{bmatrix} p \\ u \end{bmatrix}_t + \begin{bmatrix} 0 & K_0(x) \\ \frac{1}{\rho_0(x)} & 0 \end{bmatrix} \begin{bmatrix} p \\ u \end{bmatrix}_x = \mathbf{0},$$

This is a linear system  $q_t + Aq_x = 0$ . The eigenvalues and eigenvectors of A are :

$$\lambda^{1} = -c_{0}(x), \ \lambda^{2} = c_{0}(x), \ c_{0} = \sqrt{K_{0}/\rho_{0}(x)}$$
$$r^{1} = \begin{bmatrix} -Z_{0}(x) \\ 1 \end{bmatrix}, \ r^{2} = \begin{bmatrix} -Z_{0}(x) \\ 1 \end{bmatrix}$$

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General solution to linear acoustics problem:

$$\begin{bmatrix} p(x,t) \\ u(x,t) \end{bmatrix} = w^1(x-\lambda^1 t)r^1 + w^2(x-\lambda^2 t)r^2$$

where  $w^1 \mbox{ and } w^2$  are dependent upon the initial condition and are found by setting  ${\bf t}={\bf 0}$  and solving

$$Rw = q_0$$

where R is the matrix of eigenvectors of A.

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### **Riemann Problem for Linear Acoustics**

### Consider

We can represent the right and left states as linear combinations of the eigenvectors

$$q_r = w_r^1 r^1 + w_r^2 r^2 \text{ and } q_l = w_l^1 r^1 + w_l^2 r^2$$

The jump in q across the interface can be written as

$$(q_r - q_l) = \alpha^1 r^1 + \alpha^2 r^2 = \mathcal{W}^1 + \mathcal{W}^2$$

We can get alpha by solving  $R\alpha = (q_r - q_l)$ . Combining these equations and solving for the middle state:

$$q^*(x,t) = ql + \alpha^1 r^1 = q_r - \alpha^2 r^2$$

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- ▶ Reconstruct a piecewise polynomial function q̃<sup>n</sup>(, t<sub>n</sub>) defined for all x, from the cell averages Q<sub>i</sub><sup>n</sup>.
- Evolve the hyperbolic equation exactly (or approximately) with this initial data to obtain q̃<sup>n</sup>(x, t<sub>n+1</sub>) at the next time step. (Solve the Riemann problem at the cell interfaces!)
- Average this function over each grid cell to obtain new cell averages.

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We would like our model for ESWT to:

- Capture wave behavior at sharp interfaces due to inhomogeneities
- Be able to represent weak shock wave as discontinuities
- Handle varying material parameters
- Model propagation of specific ESWT pressure wave form

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- There are two types of waves in a solid body:
  - P-waves are a result of compression or normal stresses
  - S-waves are a result of shearing
- Modeling these waves gives information about compression, tension and shear in the physical system.
- In water there are no shear waves and the linear elasticity equations are equivalent to acoustics.

IDEA: Model pressure wave in ESWT using elasticity equations.

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### **Elasticity Equations**

The linear elasticity equations are a result of assuming a linear relationship between the stress and strain (Hooke's law). The 3D Linear Elasticity Equations are:

$$\begin{split} \sigma_t^{11} & -(\lambda+2\mu)u_x - \lambda v_y - \lambda w_z = 0 & \text{ESWT} \\ \text{Background} \\ \sigma_t^{22} & -\lambda u_x - (\lambda+2\mu)v_y - \lambda w_z = 0 & \text{Numerical met} \\ \sigma_t^{33} & -\lambda u_x - \lambda v_y - (\lambda+2\mu)w_z = 0 & \text{of ESWT} \\ & \sigma_t^{12} - \mu(v_x+u_y) = 0 & \text{Elasticity Equation} \\ & \sigma_t^{23} - \mu(v_z+w_y) = 0 & \text{Elasticity Equation} \\ & \sigma_t^{31} - \mu(u_z+w_x) = 0 & \text{Future Work} \\ & \rho u_t - \sigma_x^{11} - \sigma_y^{12} - \sigma_z^{13} = 0 & \\ & \rho w_t - \sigma_x^{13} - \sigma_y^{23} - \sigma_z^{33} = 0 & \\ \end{split}$$

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### Elasticity Equations - Linear System

This system can be written as

$$q_t + Aq_x + Bq_y + Cq_z = 0$$

where

The eigendecomposition of these matrices is used to find solutions to the Riemann problem.

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#### Maximum compression



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Ellipsoidal reflection, focusing of pressure wave









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Pressure wave hitting a cylindrical inclusion:









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### Limitation of Linear Elasticity Equations

No nonlinear behavior can develop in this system - we can not model the ESWT pressure wave with this system. Numerical Modeling of Extracorporeal Shock Wave Therapy with Finite Volume Methods

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### Euler Equations of Gas Dynamics

- System of equations which models compressible, inviscid flow (Navier-Stokes with no viscosity).
- Nonlinear system of equations that is able to model the ESWT wave form when using the appropriate equation of state.

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In conservative form the 3D Euler equations are:

$$q_t + f(q)_x + g(q)_y + h(q)_z = 0$$

where

$$q = \begin{bmatrix} \rho_{u} \\ \rho_{v} \\ \rho_{v} \\ \rho_{w} \end{bmatrix}, f(q) = \begin{bmatrix} \rho_{u}^{u^{2} + p} \\ \rho_{u}^{u^{2} + p} \\ \rho_{u}^{w} \\ (E + p)u \end{bmatrix},$$
$$g(q) = \begin{bmatrix} \rho_{v} \\ \rho_{v}^{v} \\ \rho_{v}^{v^{2} + p} \\ \rho_{v}^{w} \\ (E + p)v \end{bmatrix}, h(q) = \begin{bmatrix} \rho_{w} \\ \rho_{u}^{w} \\ \rho_{v}^{w} \\ \rho_{v}^{w^{2} + p} \\ (E + p)w \end{bmatrix}$$

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Here  $\rho$  is the density, p is the pressure, E is the total energy which we often decompose as  $E = \rho e + \frac{1}{2}\rho u^2$ , and e is the internal energy. These equations represent conservation of mass, momentum and energy.

# Tait equation of state (EOS)

To close the above system we need a relationship between  $\rho,$  p and e (state variables). For ESWT we use:

$$\frac{p+p_{\infty}}{p_0+p_{\infty}} = \left(\frac{\rho}{\rho_0}\right)^{\gamma}$$

which is known as the Tait or stiffened gas EOS.

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### Pressure wave form



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### Limitation of Euler equations

# Does not model solid dynamics, can not provide information about shear stresses.

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- A better model/integrated Riemann solver
- Stability issues?
- Correlation of results to experimental data
- Mapped grids for simple geometries
- Resolve memory issues
- Model shock wave behavior with 3D bone geometry

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