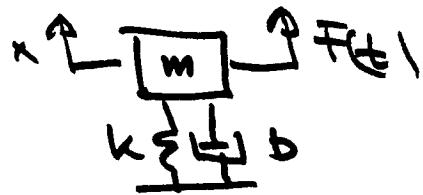


Forced Vibrations



$$\sum F = m\ddot{x} \Rightarrow m\ddot{x} + b\dot{x} + kx = F(t)$$

$$\text{if } F(t) = F_0 \sin \omega t$$

$$\ddot{x} + 2\zeta\omega_n \dot{x} + \omega_n^2 x = \frac{F_0}{m} \sin \omega t$$

$$x_p = \frac{F_0}{m} e^{i\omega t} \quad *$$

$$\text{Total response } x_T = x_H + x_P$$

where x_H = homogen. sol = free sol = transient

x_P = Particular sol = forced sol =
= Steady state soln

$$x_p = C e^{i\omega t}$$

Plug into *:

$$(-\omega^2 + 2\zeta\omega_n\omega + \omega_n^2) C e^{i\omega t} = \frac{F_0}{m} e^{i\omega t}$$

$$C = \frac{F_0/m}{(\omega_n^2 - \omega^2) + i2\zeta\omega_n\omega} e^{i\omega t}$$

or

$$x_p = \frac{F_0/m}{((\omega_n^2 - \omega^2)^2 + 4\zeta^2\omega_n^2\omega^2)^{1/2}} e^{i\omega t} \cdot e^{i\phi}$$

where $\phi = \tan^{-1} \frac{2\zeta\omega_n\omega}{\omega_n^2 - \omega^2}$

since sin wt input \rightarrow

$$x_p = \frac{F_0/m}{((\omega_n^2 - \omega^2)^2 + 4\zeta^2\omega_n^2\omega^2)^{1/2}} \cdot \sin(\omega t - \phi)$$

steady state amplitude:

$$|x_{ss}| = \frac{F_0/m}{((\omega_n^2 - \omega^2)^2 + 4\zeta^2\omega_n^2\omega^2)^{1/2}}$$

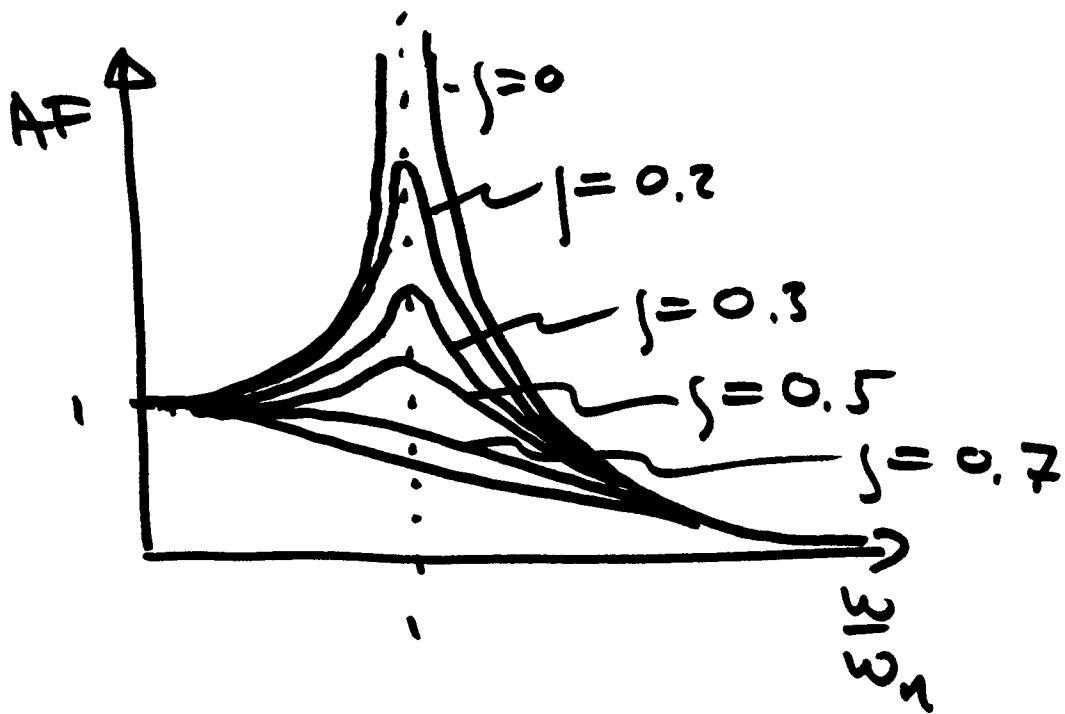
or

$$|x_{ss}| = \frac{F_0}{k} \frac{\omega_n^2}{((\omega_n^2 - \omega^2)^2 + 4\zeta^2\omega_n^2\omega^2)^{1/2}}$$

Amplification Factor =

$$= AF = \frac{\omega_n^2}{((\omega_n^2 - \omega^2)^2 + 4\zeta^2\omega_n^2\omega^2)^{1/2}}$$

$$= \frac{1}{\left[\left(1 - \left(\frac{\omega}{\omega_n} \right)^2 \right)^2 + 4\zeta^2 \left(\frac{\omega}{\omega_n} \right)^2 \right]^{1/2}}$$



The peak response will occur at

$$\frac{dAF}{d\left(\frac{\omega}{\omega_n}\right)} = 0 \Rightarrow \frac{-\frac{1}{2} \left[2 \left(1 - \left(\frac{\omega}{\omega_n} \right)^2 \right) \right] \left[-\frac{2\omega}{\omega_n} \right] + 4\zeta^2 \cdot 2 \left(\frac{\omega}{\omega_n} \right)}{\left[\zeta^3 / 2 \right]} = 0$$

$$\Rightarrow \omega \left(2\zeta^2 - 1 + \left(\frac{\omega}{\omega_n} \right)^2 \right) = 0$$

Hence $\omega = 0$ (for large ζ) or

$$2\zeta^2 - 1 + \left(\frac{\omega}{\omega_n} \right)^2 = 0 \Rightarrow$$

$$\frac{\omega}{\omega_n} = \sqrt{1 - 2\zeta^2} \leftarrow \text{Peak for small } \zeta$$

So $|s| < \frac{1}{\sqrt{2}}$ for AF to have a maximum (resonance).

$$\Rightarrow \left\{ \begin{array}{l} AF_{\max} = \frac{1}{2s(1-s^2)^{1/2}} \\ \phi = \tan^{-1} 1 - 2s^2 \end{array} \right.$$

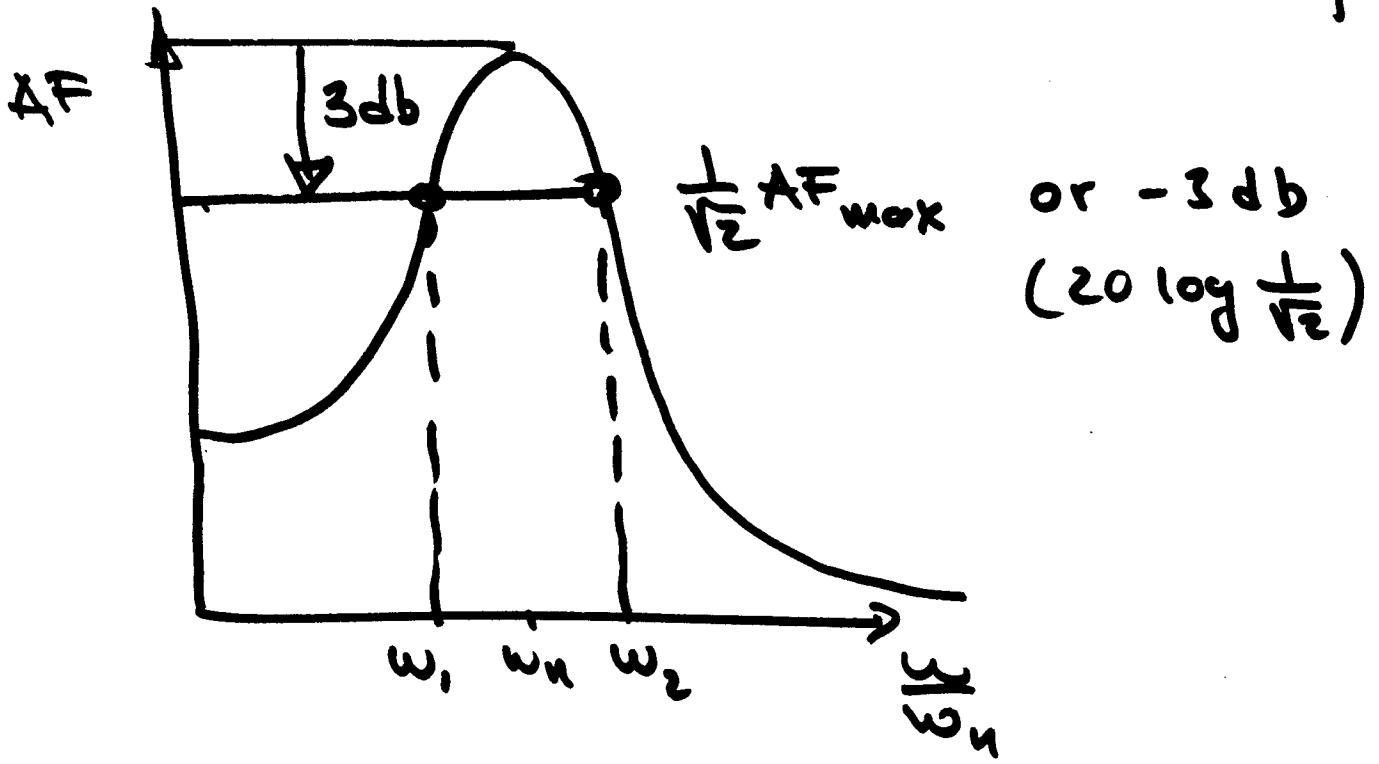
if $s \ll 1$ then

$$\boxed{AF_{\max} \approx \frac{1}{2s}} \text{ and } \phi \approx \tan^{-1} \frac{1}{s}$$

The amplification factor is $\sim \frac{1}{2s}$
 This is also called the Φ factor

$$\boxed{\Phi = \frac{1}{2s}}$$

$$s \ll 1$$



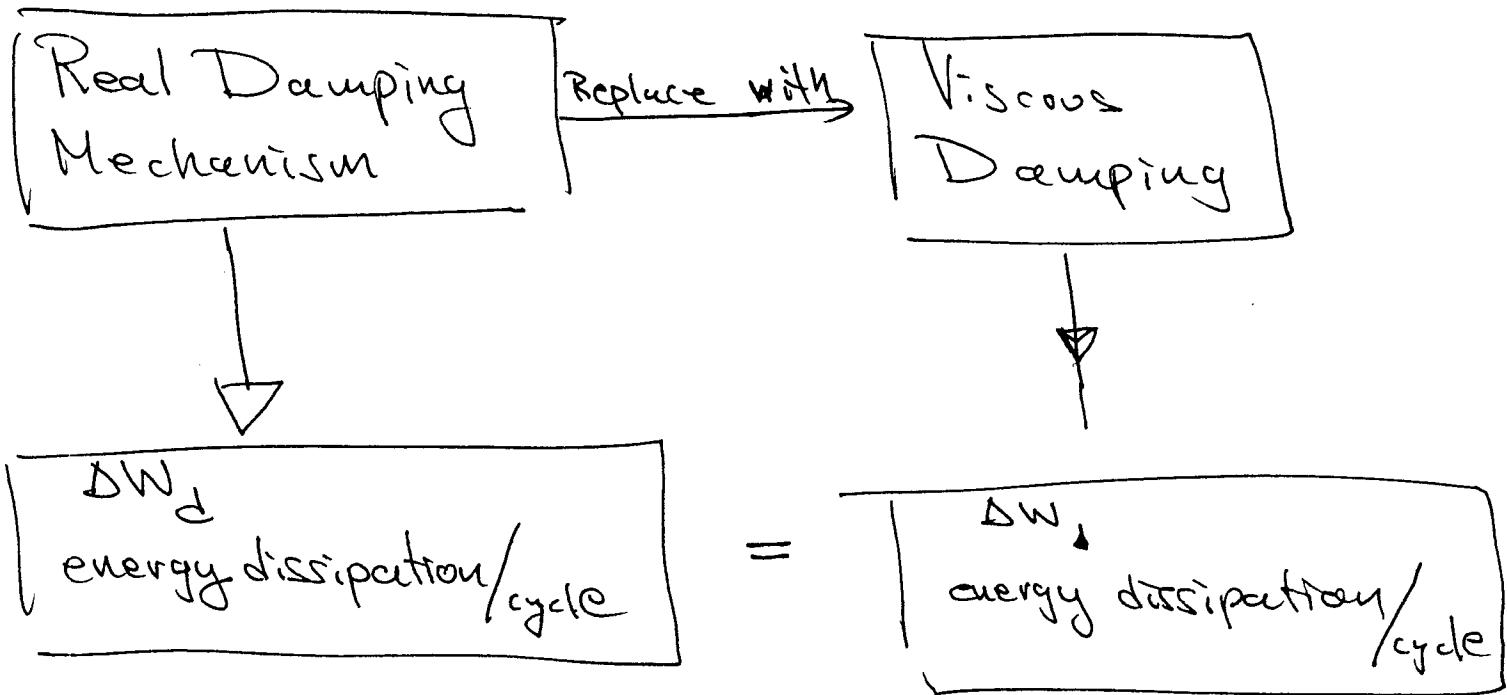
$$\omega_{1,2} = (1 \pm \zeta) \omega_n \leftarrow \text{from AF and } \zeta \ll 1$$

$$\Rightarrow \omega_2 - \omega_1 = 2\zeta \omega_n \Rightarrow \boxed{\zeta = \frac{\omega_2 - \omega_1}{2 \omega_n}}$$

$$\text{or } Q = \frac{1}{2\zeta} \Rightarrow \boxed{Q = \frac{\omega_n}{\omega_2 - \omega_1}}$$

so ζ and Q can be determined from the AF vs. $\frac{\omega}{\omega_n}$ plot.

Non Viscous Damping



For viscous damping:

$$\Delta W_d = \text{energy dissipation/cycle} = \int_{-\frac{\pi}{\omega}}^{\frac{\pi}{\omega}} F_b \cdot dx = \int_{-\frac{\pi}{\omega}}^{\frac{\pi}{\omega}} F \frac{dx}{dt} \cdot dt$$

$$\Delta W_d = \int_0^{\frac{2\pi}{\omega}} b \cdot x^2 dt = \int_0^{\frac{2\pi}{\omega}} A^2 \omega^2 \cos^2(\omega t - \phi) dt$$

$$\boxed{\Delta W_d = b A^2 \omega \pi}$$

For non-viscous damping:

Want the "equivalent viscous damper" to dissipate the input energy (at steady state)

Input : $\Delta W = \int F \cdot dx = \int_0^{2\pi/\omega} F \cdot \frac{dx}{dt} \cdot dt$

$$\Delta W = \int_0^{2\pi/\omega} F_0 \cdot \sin \omega t \cdot A_w \cos(\omega t - \phi) dt = F_0 \cdot A_w \sin \phi \left(\frac{\pi}{\omega} \right)$$

$$= \pi \cdot F_0 \cdot A \sin \phi$$

at resonance :

$$\Delta W \approx \pi \cdot F_0 \cdot A_{res}$$

so

$$b_{eq} A_{res}^2 \omega_{res} \pi = \pi \cdot F_0 \cdot A_{res}$$

$$b_{eq} = \frac{\pi \cdot F_0}{A_{res} \cdot \omega_{res} \cdot \pi}$$

Ex

