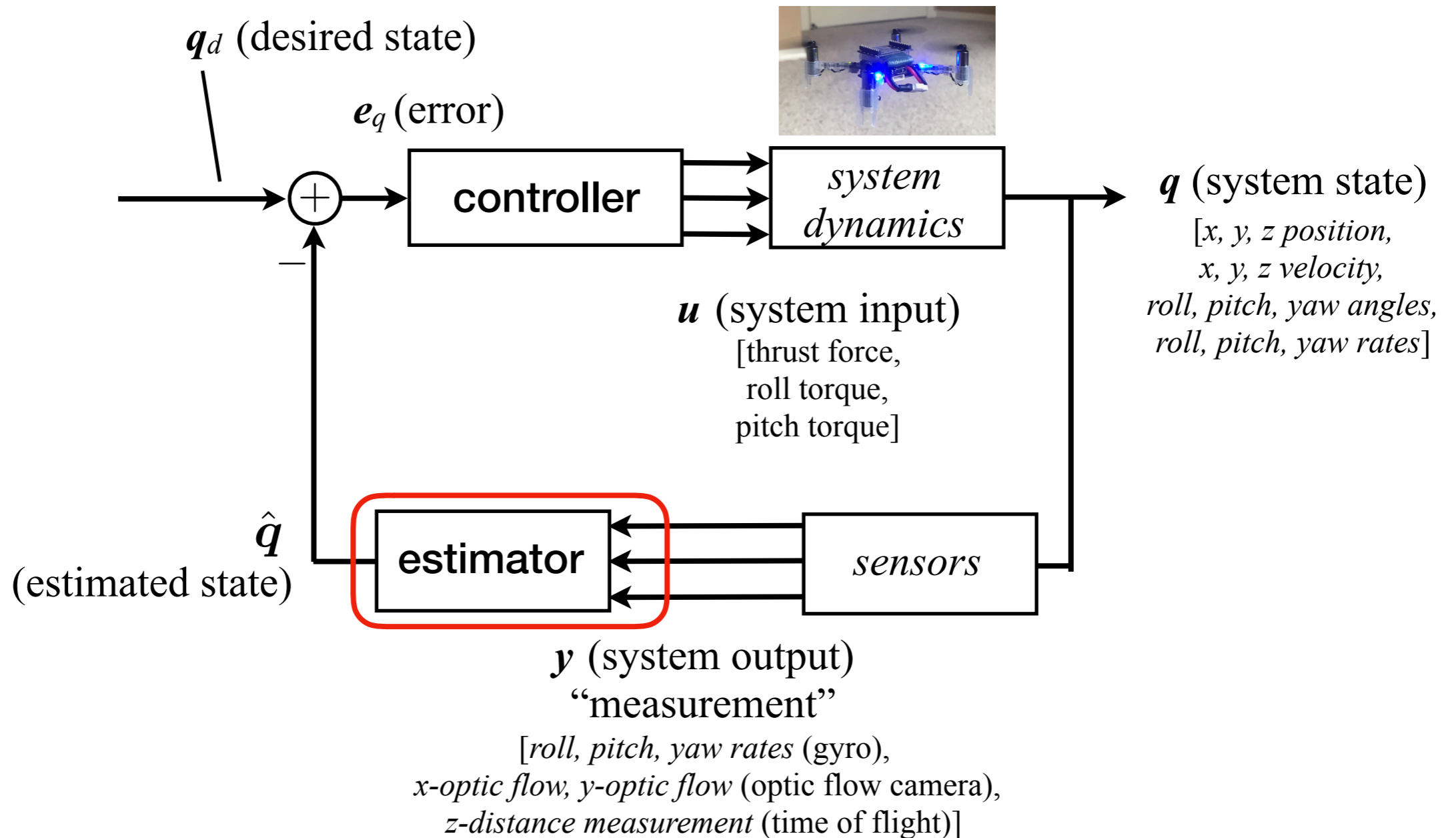
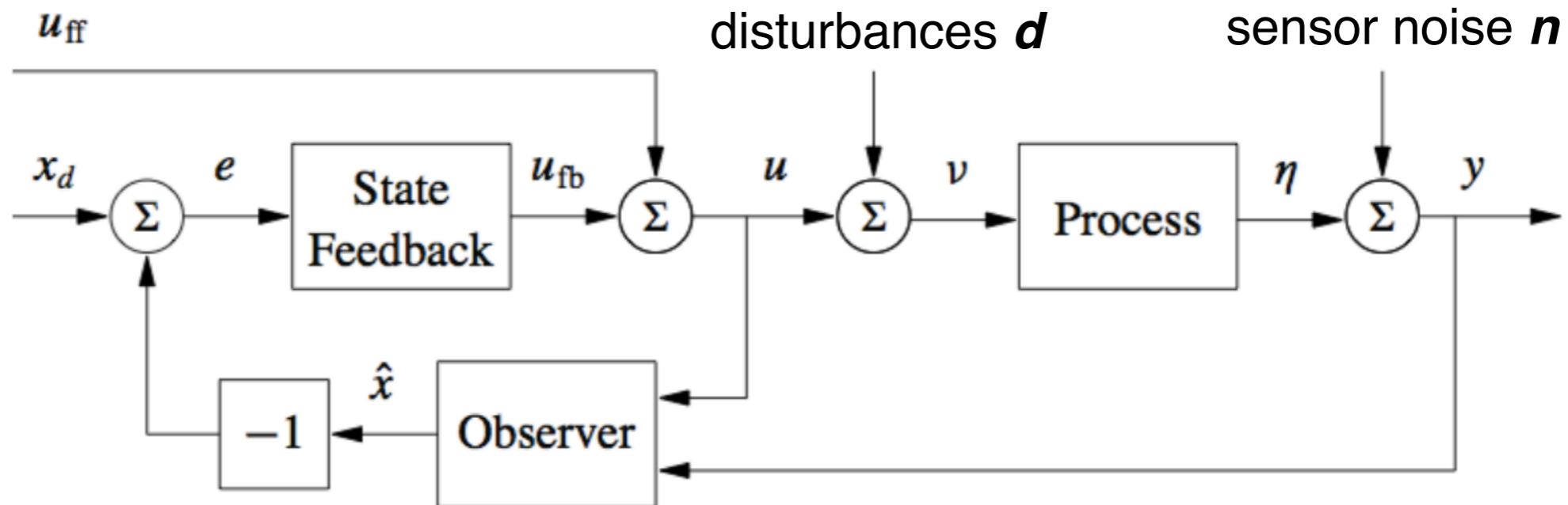


the control task



- estimator must reconstruct state vector from limited sensor information (number of sensors is typically $<$ number of states)
- *separation principle* states that controller and estimator can be designed independently

State estimation for control



Problem Setup

- Given a dynamical system with noise and uncertainty, estimate the state

$$\dot{x} = Ax + Bu + Gd$$

$$y = Cx + n$$

$$\hat{\dot{x}} = \alpha(\hat{x}, y, u) \leftarrow \text{estimator}$$

$$\lim_{t \rightarrow \infty} E(x - \hat{x}) = 0$$

- \hat{x} is called the *estimate* of x

\leftarrow expected value

Remarks

- Several sources of uncertainty: noise, disturbances, process, initial condition
- Uncertainties are unknown, except through their effect on measured output
- First question: when is this even *possible*?

Observability

Defn A dynamical system of the form

$$\dot{x} = f(x, u)$$

$$y = h(x, u)$$

is *observable* if for any $T > 0$ it is possible to determine the state of the system $x(T)$ through measurements of $y(t)$ and $u(t)$ on the interval $[0, T]$

Remarks

- Observability must respect *causality*: only get to look at past measurements
- We have ignored noise, disturbances for now \Rightarrow estimate exact state
- Intuitive way to check observability:

$$\dot{x} = Ax + Bu$$

$$y = Cx$$

$$y = \underline{Cx}$$

$$\dot{y} = C\dot{x} = \underline{CAx} + CBu$$

$$\ddot{y} = \underline{CA^2x} + CABu + CB\dot{u}$$

$$\vdots$$

$$W_o = \begin{bmatrix} C \\ CA \\ CA^2 \\ \vdots \\ CA^{n-1} \end{bmatrix}$$

Thm A linear system is observable if and only if the observability matrix W_o is full rank

State estimation: observer

Given that a system is observable, how do we actually estimate the state?

- Key insight: if current estimate is correct, follow the dynamics of the system

$$\begin{aligned} \dot{x} &= Ax + Bu \\ y &= Cx \end{aligned} \quad \hat{\dot{x}} = \underbrace{A\hat{x} + Bu}_{\text{prediction (copy of dynamics)}} + L(y - C\hat{x}) \leftarrow \text{correction (based on output error)}$$

- Modify the dynamics to correct for error based on a linear feedback term
- L is the *observer gain matrix*; determines how to adjust the state due to error
- Look at the error dynamics for $\tilde{x} = x - \hat{x}$ to determine how to choose L :

$$\dot{\tilde{x}} = \dot{x} - \dot{\hat{x}} = Ax + Bu - (A\hat{x} + Bu + LC(x - \hat{x})) = (A - LC)\tilde{x}$$

Thm If the pair (A, C) is observable (associated W_o is full rank), then we can place the eigenvalues of $A - LC$ arbitrarily through appropriate choice of L .

How to choose gain L ?

- “Kalman Filter” formulation: given system

$$\dot{\mathbf{q}} = \mathbf{A}\mathbf{q} + \mathbf{B}\mathbf{u} + \mathbf{G}\mathbf{d}$$

$$\mathbf{y} = \mathbf{C}\mathbf{q} + \mathbf{n}$$

where \mathbf{d} is process noise (“disturbance”), \mathbf{n} is sensor noise.

\mathbf{d} and \mathbf{n} are zero-mean white Gaussian noise (eg for scalar d , $p(d) = \frac{1}{\sqrt{2\pi\sigma_d^2}} e^{-\frac{1}{2}\left(\frac{d}{\sigma_d}\right)^2}$)
and $E\{\mathbf{d}\mathbf{d}^T\} = \mathbf{Q}_N = \mathbf{Q}_N^T \geq 0$ $E\{\mathbf{n}\mathbf{n}^T\} = \mathbf{R}_N = \mathbf{R}_N^T > 0$

- if noise is “stationary” (not changing with time) then the Kalman gain L minimizes expected squared error of the state estimate

$$\hat{\mathbf{q}} = \mathbf{A}\hat{\mathbf{q}} + \mathbf{B}\mathbf{u} + \mathbf{L}(\mathbf{y} - \mathbf{C}\hat{\mathbf{q}})$$

Remarks

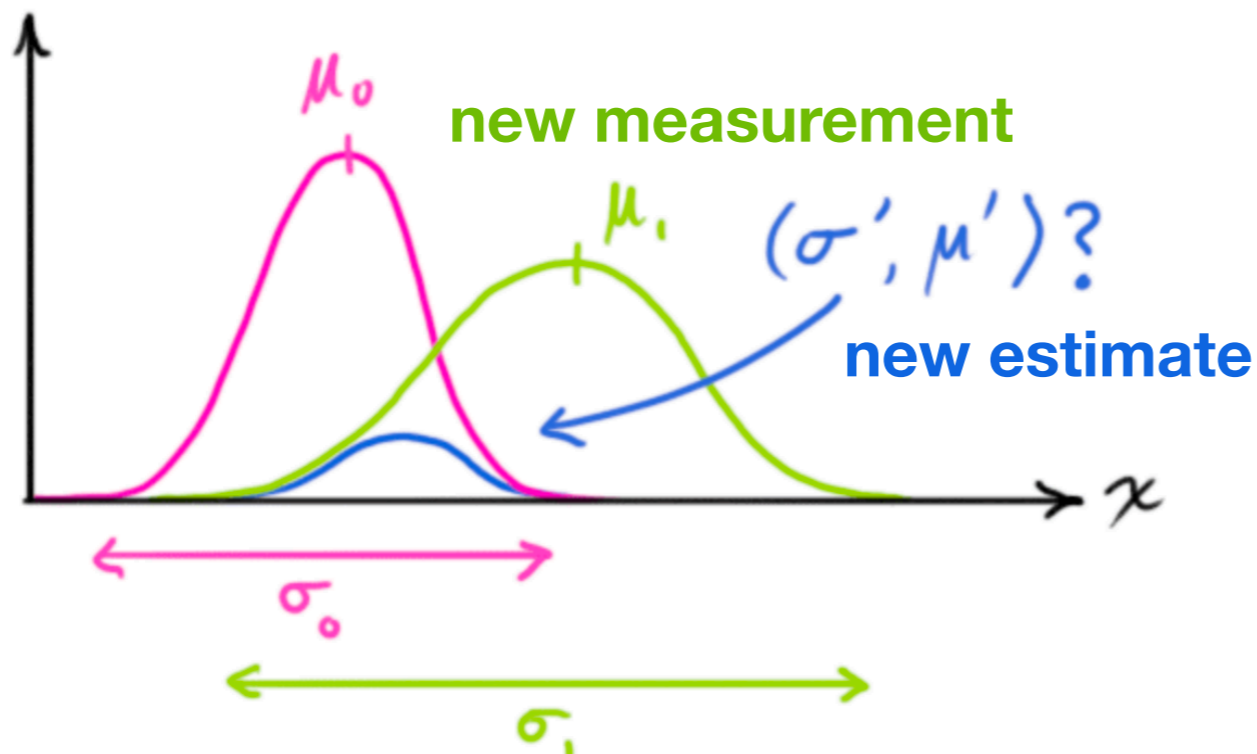
- L is *also* the solution to an algebraic Riccati equation
 - use `lqe(A, B, G, QN, RN)` or `MATLAB lqe(A, B, Q, R)`
- Can choose other L 's, but Kalman L minimizes error noise

intuition

- Kalman Filter combines information from dynamics prediction with information sensor measurements using a “bayesian update”
 - multiply the probability density function (PDF) of the state estimate by the PDF of the new measurement

1D case

prediction from
dynamics model (“prior”)



Bayesian inference:
new PDF = prior PDF * measurement PDF

$$\mu' = \mu_0 + \frac{\sigma_0^2(\mu_1 - \mu_0)}{\sigma_0^2 + \sigma_1^2}$$
$$\sigma'^2 = \sigma_0^2 - \frac{\sigma_0^4}{\sigma_0^2 + \sigma_1^2}$$

(KF does this for n dimensions)

remarks

- matrices Q_N and R_N are usually diagonal, meaning noise is not correlated
- sensor noise matrix R_N can come from datasheet or can be estimated:

$$R_N = \begin{bmatrix} \sigma_{n1}^2 & 0 & \dots \\ 0 & \sigma_{n2}^2 & \\ \vdots & & \ddots \end{bmatrix} \quad \sigma_n = \sqrt{\frac{1}{N-1} \sum_i (y_i - y_{i,m})^2} \quad \begin{array}{l} y_{i,m} \text{ is sensor's measurement} \\ y_i \text{ is ground truth measurement} \end{array}$$

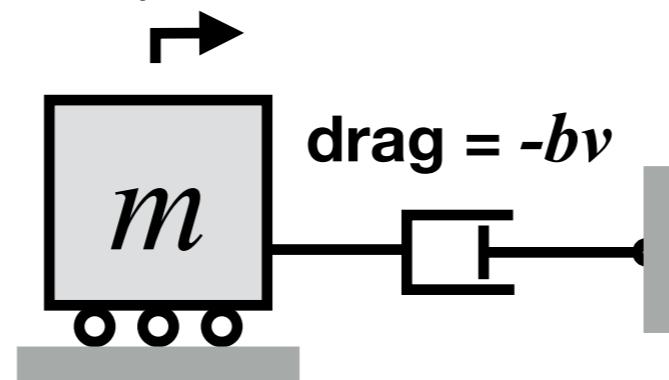
`= numpy.linalg.std(ym-y)` if y 's are arrays of data

- disturbance noise Q_N is harder to measure. Perspective: is tuning knob
- large disturbance $Q_N \Rightarrow$ trust sensors more than prediction \Rightarrow large L
- small disturbance $Q_N \Rightarrow$ trust prediction more than sensors \Rightarrow small L
- linear KF requires very little computation, just a few matrix multiply operations
- rose to prominence on the Moon Lander in the 1960's (!)
- important variants:
 - sensors that do not update at equal intervals: use “information form” that separates prediction from correction step, using different L for each sensor
 - for nonlinear system, use extended KF (“EKF”) (see Murray, Optimization-Based Control) or unscented KF (“UKF”) (more computation needed)
 - crazyflie uses an extended KF to enable more aggressive maneuvers (Greif2017 on course website)

Example: me586_example_kalman_estimator.ipynb

A) Kalman Filter to estimate velocity from this dynamical system:

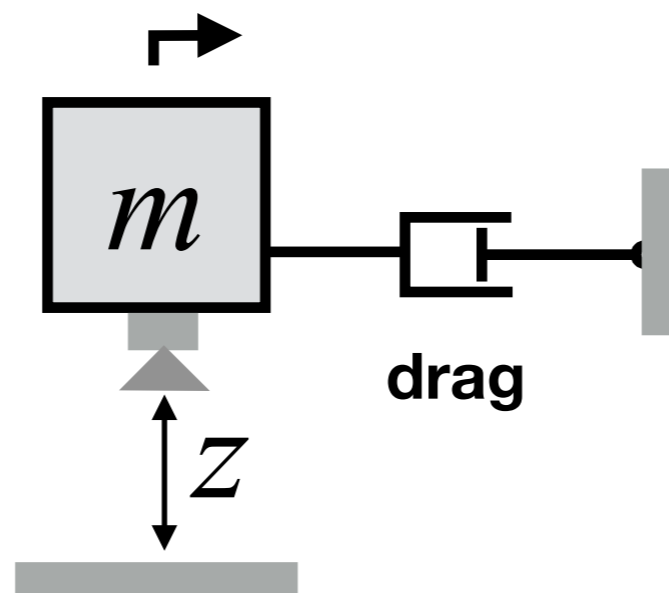
$$v_m = v + n \quad (\text{vel measurement} = \text{true value} + \text{noise})$$



B) Vary tuning knob Q_N (magnitude of disturbance noise)

C) helicopter-based optic flow (must linearize at desired height $z=z_d$)

$$v_m = \Omega_m z + n$$



compared to a low-pass filter, the Kalman Filter:

- can estimate “hidden” but observable states
- can perform sensor fusion between different sensors at different update rates
- can accommodate effect of known inputs
- reduces estimate lag time, if the quantity you are interested in behaves as a dynamical system
- minimizes expected squared estimate error
- but needs a model of dynamics

well-suited to a dynamical system such as an aircraft with a good model (eg N-E equations) and states that are not directly measured by sensors (e.g. orientation)

The separation principle

Feedback the estimated state: $u = -K\hat{x} + k_r r$ driving the output y to the value r is another way to do trajectory tracking

- **Analysis:** Again, let $\tilde{x} = x - \hat{x}$ denote the error in the state estimate. The dynamics of the controlled system under this feedback are:

$$\begin{aligned}\dot{x} &= Ax + Bu = Ax - BK\hat{x} - Bk_r r = Ax - BK(x - \tilde{x}) + Bk_r r \\ &= (A - BK)x + BK\tilde{x} + Bk_r r\end{aligned}$$

- Introduce a new *augmented* state: $q = [x \quad \tilde{x}]^T$. The dynamics of the system defined by this state is:

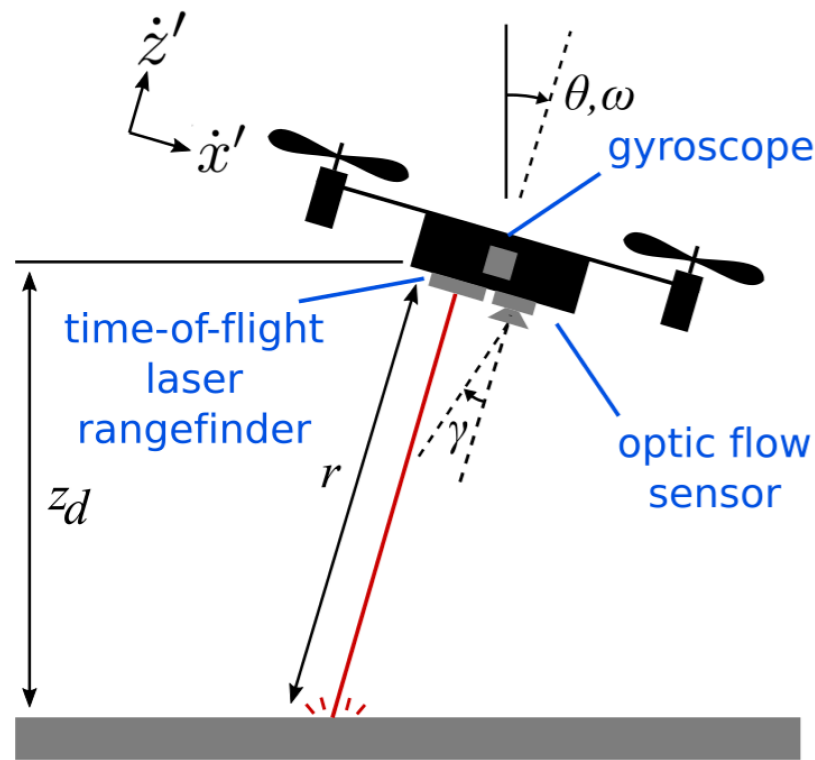
$$\begin{bmatrix} \dot{x} \\ \dot{\tilde{x}} \end{bmatrix} = \begin{bmatrix} (A - BK) & BK \\ 0 & (A - LC) \end{bmatrix} \begin{bmatrix} x \\ \tilde{x} \end{bmatrix} + \begin{bmatrix} Bk_r \\ 0 \end{bmatrix} r \equiv Mq + B_M r$$

The characteristic polynomial of M is:

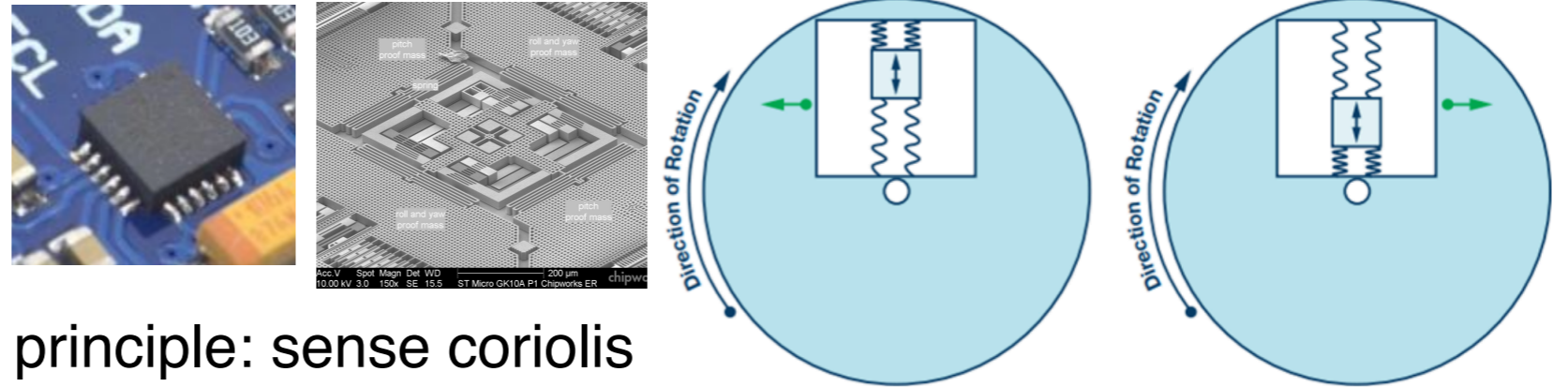
$$\lambda_M(s) = \det(sI - A + BK) \det(sI - A + LC)$$

- If the system is *observable* and *reachable*, then the poles of $(A - BK)$ and $(A - LC)$ can be set *arbitrarily and independently*
- If K is an LQR controller and L is a Kalman Filter, then is a “Linear Quadratic Gaussian” (LQG) controller

sensors



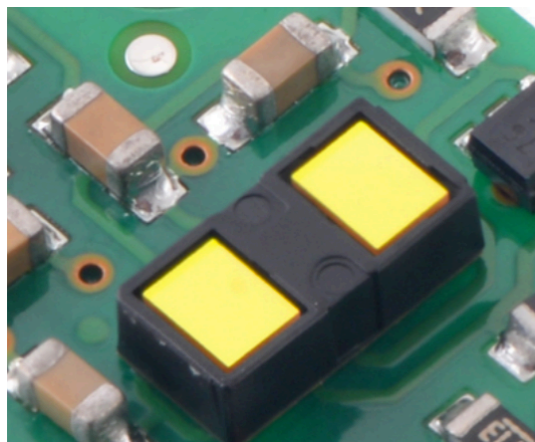
Gyroscope: Bosch BMI088



principle: sense coriolis forces using a rotating, vibrating proof mass

$$\omega_m = \omega + n_g$$

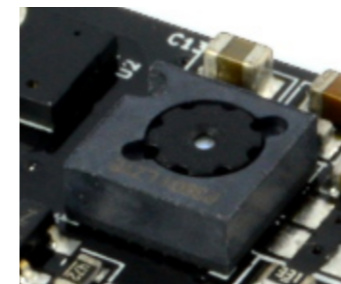
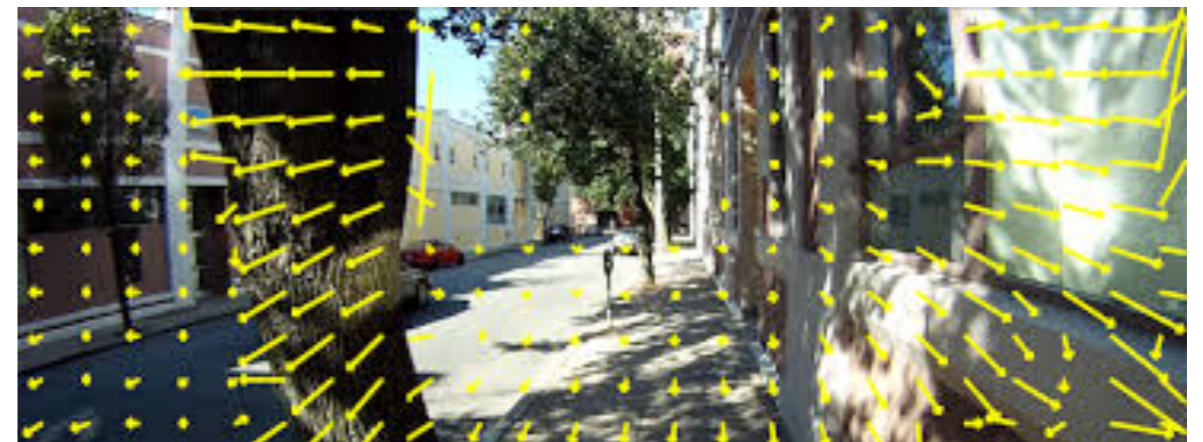
Time-of-flight laser rangefinder: ST VL53L1



principle: measure time taken for laser light to reflect

model for sensor: $r_m = r + n_t$ **noise**

Optic flow sensor: Pixart PMW3901



principle: measure speed of motion of visual scenery directly below to estimate lateral velocity

$$\Omega_m = \Omega + n_o = -\omega + \frac{1}{r}(\dot{x}' \cos \gamma - \dot{z}' \sin \gamma) + n_o$$

(derive on board)