

Physics 514, Electrodynamics II
Department of Physics, University of Washington
Winter quarter 2020
March 11, 2020, 11am
On-line lecture

Administrative

Homework 9 due Friday, March 11, 11am. Slide HW under my office door C503 or scan and send it via email.

No final exam.

MRE postponed to early Spring quarter.

Lecture

Jackson Chapter 8: Waveguides & resonant cavities

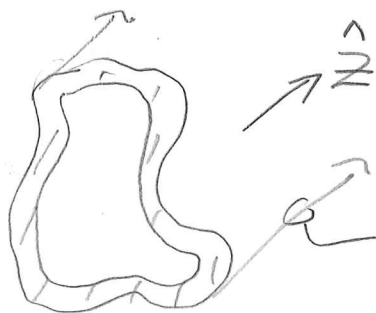
J.C.8.1 Fields at the surface and within a conductor. We'll come back to this. This section is important when the waveguide walls are lossy.

J.C.8.2 Cylindrical cavities and waveguides. Actually, this is a generic discussion of how to set up a waveguide problem.

J.C.8.3. Waveguides. Brief discussion of TEM waveguides.

J.C.8.4 Modes in a rectangular waveguide. We'll also evaluate the corresponding circular waveguide.

WAVEGUIDES II: JACKSON § 8.2-4



VACUUM INSIDE,
WALLS ARE PERFECT CONDUCTOR,
CONSTANT CROSS-SECTION.

ASSUME HARMONIC (ω) WAVES.

MAXWELL'S EQUATION LEAD TO THE
HELMHOLTZ EQUATION

$$\left(\nabla^2 + \frac{1}{c^2} \omega^2 \right) \begin{Bmatrix} \vec{E} \\ \vec{B} \end{Bmatrix} = 0$$

WITH SOLUTIONS

$$\begin{Bmatrix} \vec{E}(\vec{r}, t) \\ \vec{B}(\vec{r}, t) \end{Bmatrix} = \begin{Bmatrix} \vec{E}(x, y) \\ \vec{B}(x, y) \end{Bmatrix} e^{i(\pm kz - \omega t)}$$

WHERE WE ANTICIPATED PROPAGATION
ALONG \hat{z} .

WE WILL NEED TO FIND THE
WAVE NUMBER k . (THE "GUIDED
WAVE NUMBER".)

THE z-DIRECTION IS SPECIAL, SO WE SEPARATE FIELDS AND EQUATIONS INTO PARTS ALONG \hat{z} , AND PARTS TRANSVERSE TO \hat{z} .

$$\vec{\nabla} = \vec{\nabla}_t + \hat{z} \frac{\partial}{\partial z}$$

$$\vec{E} = \vec{E}_t + \vec{E}_z$$

$$\vec{B} = \vec{B}_t + \vec{B}_z$$

LET'S ALSO SEPARATE MAXWELL'S EQUATIONS, E.G.,

$$\vec{\nabla} \times \vec{B} = -i \frac{1}{c^2} \omega \vec{E} \quad \text{BECOMES}$$

$$\begin{aligned} (\vec{\nabla}_t + \hat{z} \frac{\partial}{\partial z}) \times (\vec{B}_t + \vec{B}_z) \\ = -i \frac{1}{c^2} \omega (\vec{E}_t + \vec{E}_z). \end{aligned}$$

THE ABOVE MAXWELL EQUATION EMBEDS LONGITUDINAL AND TRANSVERSE PARTS,

HERE'S THE TRANSVERSE PART:

$$\underbrace{\vec{\nabla}_t \times \vec{B}_z + \hat{z} \frac{d}{dz} \times \vec{B}_t}_{-\hat{z} \times (-\vec{\nabla}_t B_z)} = \underbrace{-i \frac{1}{c^2} \omega \vec{E}_t}_{\hat{z} \times (-i \frac{1}{c^2} \omega \hat{z} \times \vec{E}_t)}$$

$$\underbrace{\phantom{\vec{\nabla}_t \times \vec{B}_z + \hat{z} \frac{d}{dz} \times \vec{B}_t}}_{\hat{z} \times \frac{d}{dz} \vec{B}_t}$$

* SEE JACKSON EQN 8.22

ALTHOUGH NOT FORMALLY CORRECT;
DROP THE LEADING " $\hat{z} \times \dots$ ", YIELDING

$$-\vec{\nabla}_t B_z + \frac{d}{dz} \vec{B}_t = -i \frac{1}{c^2} \omega \hat{z} \times \vec{E}_t$$

* JACKSON EQN. 8.24 (LEFT),

THERE ARE 3 OTHER SIMILAR EQUATIONS.

IF YOU PROVIDE \vec{E}_z AND \vec{B}_z ,
THE FOUR EQUATIONS PROVIDE
SOLUTIONS TO THE 4 COMPONENTS
OF \vec{E}_t AND \vec{B}_t .

SEE JACKSON EQUATIONS 8.26a-b.



So, WAVEGUIDE PROBLEMS REDUCE TO FINDING \vec{E}_z AND \vec{B}_z . BY THEMSELVES, \vec{E}_z AND \vec{B}_z PROVIDE INFORMATION ABOUT THE "MODE STRUCTURE", CUTOFF FREQUENCIES, ETC,

COMMENT I: WITH SMOOTH WALL, GOOD CONDUCTOR, CONSTANT CROSS-SECTION, 3 TYPES OF MODES.

TE "TRANSVERSE ELECTRIC"

$$E_z = 0 \text{ EVERYWHERE.}$$

TM "TRANSVERSE MAGNETIC"

$$B_z = 0 \text{ EVERYWHERE.}$$

TEM "TRANSVERSE ELECTRO-MAGNETIC"

$$E_z = 0, B_z = 0 \text{ EVERYWHERE.}$$

5

SPECIAL CASE: TEM MODES
(JACKSON P. 358).

- SKIN DEPTH IS VERY SMALL FOR A GOOD CONDUCTOR, SO CURRENTS \vec{K} ARE PARALLEL TO THE SURFACE.
- THE BOUNDARY CONDITION ON \vec{H} IMPLIES \vec{H} IS PARALLEL TO THE SURFACE, AS WELL.
- BUT FOR TEM MODES, \vec{H} IS TRANSVERSE. FROM $\vec{H}_1 - \vec{H}_2 = \vec{K} \times \hat{n}$, THE CURRENTS \vec{K} ARE ALONG \hat{z} .
- SINCE $\vec{K} \sim \hat{z}$, $\vec{A} \sim \hat{z}$.
- SO THE ELECTRIC FIELD $\vec{E} = -\vec{\nabla}\Phi - \frac{d}{dt}\vec{A}$ BECOMES
$$\vec{E} = -\vec{\nabla}_t \Phi - \hat{z} \frac{d}{dz} \Phi - \frac{d}{dt} \vec{A}$$
 SINCE $E_z = 0$, THE LAST 2 TERMS SUM TO ZERO.

WE ARE LEFT WITH

$\vec{E} = -\vec{\nabla}_t \Phi$; THIS IS 2D ELECTROSTATICS,

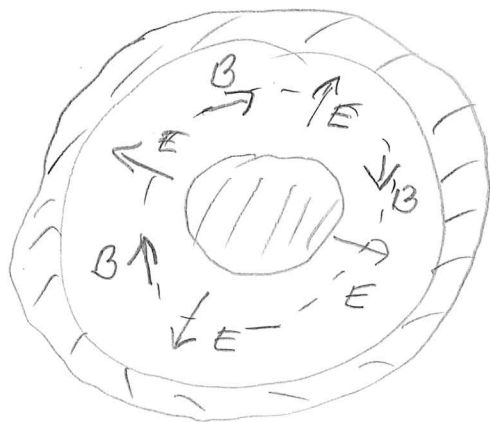
WE STILL HAVE MAXWELL'S EQUATIONS, WHICH GIVE

$$\vec{B} = \frac{1}{c} \hat{z} \times \vec{E}$$

TO GET THE SIGNS RIGHT, YOU'LL NEED $\vec{E} \times \vec{B}$ TO BE ALONG THE PROPAGATION DIRECTION,

JACKSON EQ N 8, 28.

EXAMPLE: COAX CABLE; TEM MODE



AT A FIXED POSITION AT A FIXED TIME,

VARY POSITION;

e^{ikz}

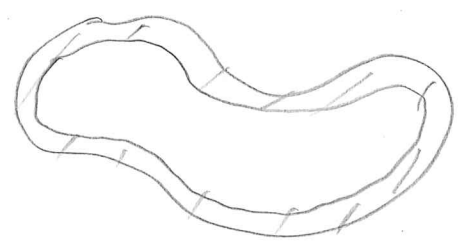
VARY TIME

$e^{i\omega t}$

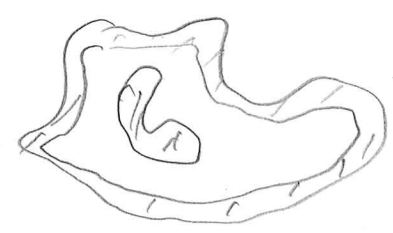
DISPERSION RELATION IS $k^2 = \frac{1}{c^2} \omega^2$!
NO CUTOFF.

TEM CONTINUED,
HOW MANY CONDUCTORS?

START WITH 1 CONDUCTOR:



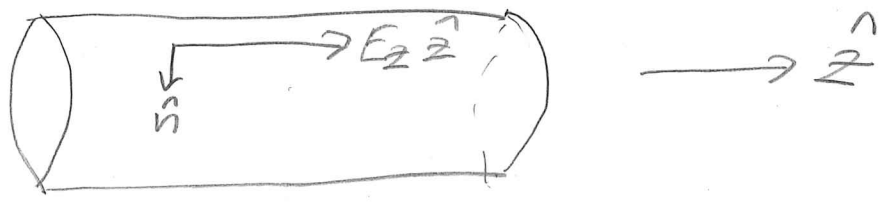
- ON THE INTERIOR SURFACE,
 $\vec{E}_{||} = 0$ (THE \vec{E} FIELD IS "NORMAL").
- HENCE, A LINE INTEGRAL BETWEEN ANY TWO POINTS a, b ON THE CROSS-SECTION SURFACE IS ZERO. HENCE, THE SURFACE CROSS-SECTION IS AN EQUIPOTENTIAL. HENCE $\vec{E} = 0$ EVERYWHERE.
- YOU NEED 2 OR MORE SURFACES TO HAVE A TEM WAVEGUIDE:



BACK TO GENERAL COMMENTS ON
TE, TM AND TEM MODES.

WE WISH TO FIND THE BOUNDARY
CONDITIONS IN TERMS OF E_z
AND B_z .

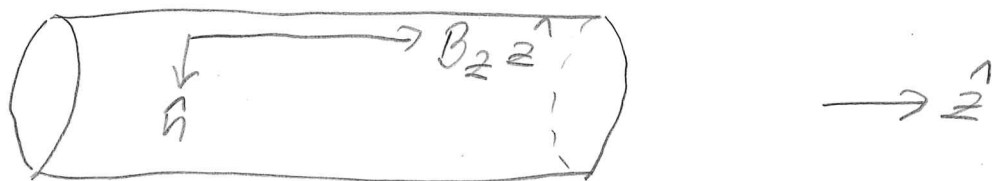
i. E_z BOUNDARY CONDITION.



$$\vec{E}|_s \sim \hat{n}, \text{ so } E_z|_s = 0$$

JACKSON EPN, 8.29.

ii. B_z BOUNDARY CONDITION.



THIS IS TRICKIER. RECALL

$$-\vec{\nabla}_t B_z + \frac{d}{dz} \vec{B}_t = -i \frac{1}{c^2} \omega \hat{z} \times \vec{E}_t.$$

- PICK A POINT ON THE SURFACE.
- TAKE THE PROJECTION OF EACH TERM ALONG \hat{n} .

$$(-\vec{\nabla}_t B_z) \cdot \hat{n} \Big|_s + \left(\frac{d}{dz} \vec{B}_t \right) \cdot \hat{n} \Big|_s$$

$$= \left(-i \frac{1}{c^2} \omega \hat{z} \times \vec{E}_t \right) \cdot \hat{n} \Big|_s$$

• • THE SECOND TERM $(\vec{B}_t \cdot \hat{n})$ VANISHES (WHY?)

• • FOR THE LAST TERM, RECALL $\vec{E}_{\parallel} \Big|_s = 0$. SO $\vec{E}_t \sim \hat{n}$.

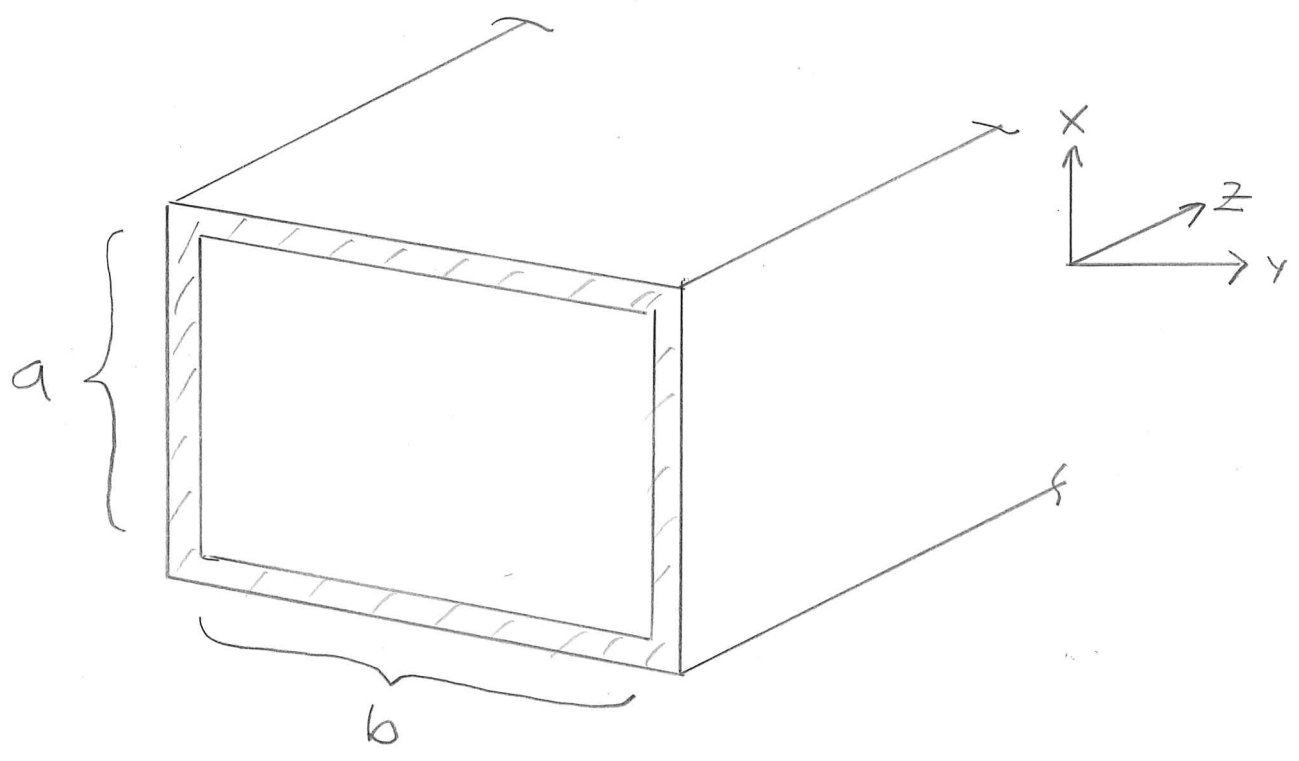
SO $\hat{z} \times \vec{E}_t$ IS ORTHOGONAL

TO \hat{n} . SO THE LAST TERM VANISHES, LEAVING

$$\vec{\nabla}_t B_z \cdot \hat{n} \Big|_s = 0, \text{ OR } \frac{d}{dz} B_z \Big|_s = 0$$

JACKSON EQN. 8.30.

EXAMPLE; RECTANGULAR WAVEGUIDE,
TE MODES.



THE HELMHOLTZ EQUATION

$$\left(\nabla^2 + \frac{1}{c^2} \omega^2 \right) \begin{Bmatrix} \vec{E} \\ \vec{B} \end{Bmatrix} = 0$$

BECOMES, FOR E_z AND B_z :

$$\left(\nabla_t^2 + \left(-k^2 + \frac{1}{c^2} \omega^2 \right) \right) \begin{Bmatrix} E_z \\ B_z \end{Bmatrix} = 0$$

FOR TE MODES, $E_z = 0$.

IN CARTESIAN COORDINATES, THE
THE HELMHOLTZ EQUATION IS

$$\left(\frac{d^2}{dx^2} + \frac{d^2}{dy^2} + \left(-k^2 + \frac{\omega^2}{c^2} \right) \right) B_z = 0$$

AS USUAL, WE SEPARATE VARIABLES!

ASSUME $B_z(x,y) = X(x)Y(y)$. IF WE FIND A SOLUTION, THE SEPARATION IS JUSTIFIED (AS WE KNOW IS THE CASE).

$$\frac{1}{X} \frac{d^2}{dx^2} X + \frac{1}{Y} \frac{d^2}{dy^2} Y + \left(-k^2 + \frac{\omega^2}{c^2} \right) = 0$$

EACH O.D.E. IS SEPARATELY CONSTANT:

$$\frac{1}{X} \frac{d^2}{dx^2} X = -k_x^2, \quad \frac{1}{Y} \frac{d^2}{dy^2} Y = -k_y^2$$

$$\text{WITH } -k_x^2 - k_y^2 + \left(-k^2 + \frac{\omega^2}{c^2} \right) = 0$$

[THE TERM IN PARENTHESES IS THE "CUTOFF WAVE NUMBER" k_c , FOR REASONS THAT WILL BECOME CLEAR:

$$k_c^2 \equiv -k^2 + \frac{\omega^2}{c^2}.]$$

WE GET THE USUAL SOLUTIONS

$$X(x) = X_S \sin K_x x + X_C \cos K_x x.$$

APPLY BOUNDARY CONDITIONS;

$$\frac{d}{dn} B_z |_S = 0 \text{ BECOMES}$$

$$\frac{d}{dx} B_z \Big|_{x=0}^{x=a} = 0$$

THE $x=0$ BOUNDARY CONDITION
REQUIRES $X_S = 0$,

THE $x=a$ BOUNDARY CONDITION
REQUIRES $K_x = m\pi/a$; $m = 0, 1, \dots$.

SIMILARLY

$$Y(y) = Y_C \cos K_y y \text{ WITH}$$

$$K_y = n\pi/b; \quad n = 0, 1, \dots$$

MODES ARE IDENTIFIED WITH
MODE NUMBERS m AND n ,

THE GENERIC MODE LOOKS LIKE

$$B_{z;m,n}(x,y) = B_{0,z;m,n} \cos \frac{m\pi}{a} x \cos \frac{n\pi}{b} y.$$

WHAT ARE THE PROPAGATION PROPERTIES (PHASE VELOCITY, CUTOFF FREQUENCIES, ETC.) OF THE TE_{mn} MODE?

$$\text{FROM } -k_x^2 - k_y^2 = -k^2 + \omega^2/c^2,$$

$$k^2 = \omega^2/c^2 - \frac{\pi^2 m^2}{a^2} - \frac{\pi^2 n^2}{b^2}.$$

WRITE THIS AS

$$k^2 = \omega^2/c^2 - k_c^2.$$

FOR $\omega^2/c^2 < k_c^2$, THE WAVE NO LONGER PROPAGATES. THIS DEFINES A CUTOFF FREQUENCY FOR EACH MODE $\omega_c; mn$.

k^2 LEADS TO THE PHASE VELOCITY (THE "GUIDED WAVE VELOCITY v_g ") IN THE USUAL WAY!

$$v_g^2 = \omega^2/k^2 > 1 \text{ FOR } \omega^2 > c^2 k_c^2.$$

THE FORM OF K

$$K^2 = \omega^2/c^2 - \pi^2 \frac{m^2}{a^2} - \pi^2 \frac{n^2}{b^2}$$

IS OFTEN WRITTEN

$$K^2 = \frac{1}{c^2} (\omega^2 - \omega_{c, m, n}^2)$$

SO AS TO REMEMBER THE FORM OF THE DISPERSION RELATION OF PLASMAS, ETC.

IF YOU WISH, YOU COULD FIND THE GROUP VELOCITY

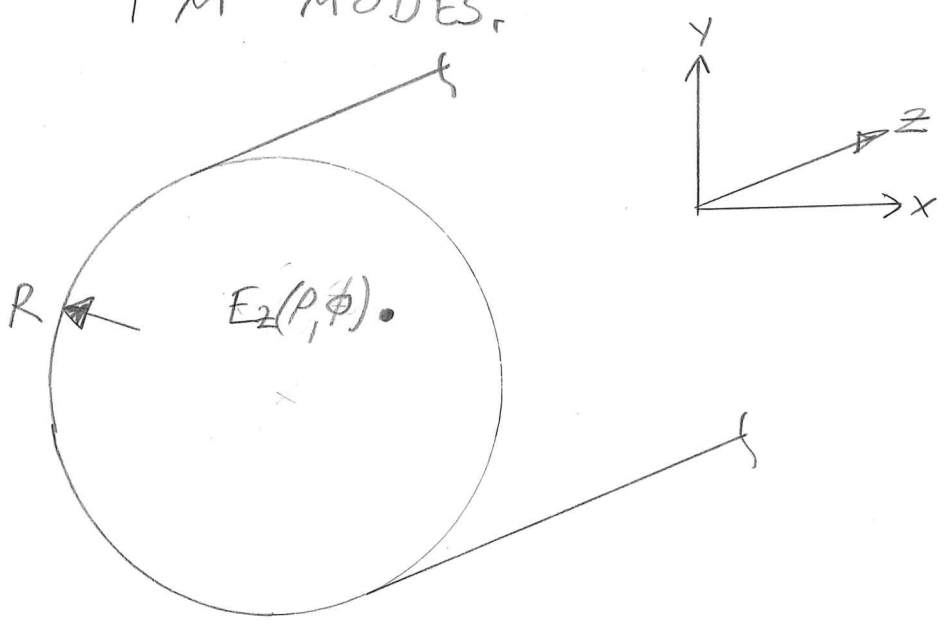
$$\frac{1}{dk/d\omega} \text{ AND FIND ITS } < c.$$

K² ALSO LEADS TO THE GUIDED WAVELENGTH: $\lambda = 2\pi/k$

$$\lambda = \frac{1}{\frac{1}{c} \omega \sqrt{1 - \frac{\omega_{c, m, n}^2}{\omega^2}}} \text{ OR}$$

$$\lambda = \lambda_0 \frac{v_g}{c} \text{ WITH } \lambda_0 \text{ THE FREE-SPACE WAVELENGTH.}$$

EXAMPLE: ROUND WAVEGUIDE,
TM MODES.



$$(\nabla_t^2 + (-k^2 + \omega^2/c^2)) E_z(\rho, \phi) = 0$$

$$\left[\frac{1}{\rho} \frac{d}{d\rho} \left(\rho \frac{d}{d\rho} \right) + \frac{1}{\rho^2} \frac{d^2}{d\phi^2} + (-k^2 + \omega^2/c^2) \right] \times E_z(\rho, \phi) = 0$$

SEPARATE VARIABLES WITH

$$E_z = R(\rho) \Phi(\phi)$$

$$\frac{1}{R} \frac{d^2 R}{d\rho^2} + \frac{1}{\rho R} \frac{dR}{d\rho} + \frac{1}{\rho^2 \Phi} \frac{d^2 \Phi}{d\phi^2} + (-k^2 + \frac{\omega^2}{c^2}) = 0.$$

Now, multiply by ρ^2 !

$$\frac{\rho^2}{R} \frac{d^2 R}{d\rho^2} + \frac{\rho}{R} \frac{dR}{d\rho} + \frac{1}{\Phi} \frac{d^2 \Phi}{d\phi^2} + \left(k^2 - \frac{\omega^2}{c^2} \right) \rho^2 = 0$$

i. THE Φ TERM IS SEPARATELY CONSTANT; $\frac{1}{\Phi} \frac{d^2 \Phi}{d\phi^2} = -k^2$

WITH SOLUTIONS

$$\Phi(\phi) = \phi_s \sin k_\phi \phi + \phi_c \cos k_\phi \phi$$

WE REQUIRE $\Phi(\phi)$ BE SINGLE-VALUED:

$$\Phi(\phi) = \Phi(\phi \pm m2\pi),$$

HENCE k_ϕ IS AN INTEGER (n).

ii THE RADIAL PIECE IS BESSEL'S EQUATION, BUT THE SOLUTION IS SIGNIFICANTLY MORE COMPLICATED DUE TO $k^2 - \omega^2/c^2$:

$$R(\rho) = C_{J,n} J_n \left(\sqrt{-k^2 + \omega^2/c^2} \rho \right) \\ + C_{N,n} N_n \left(\sqrt{-k^2 + \omega^2/c^2} \rho \right)$$

WITH J_n AND N_n BESSEL FUNCTIONS OF THE 1ST AND 2ND KIND,

THE N_n SOLUTIONS ARE SINGULAR FOR $\rho = 0$, SO ARE ABSENT,

SO FAR, WE HAVE A MODE

$$E_{z;n}(\rho, \phi) = (A_{s;n} \sin n\phi + A_{c;n} \cos n\phi) \\ \times J_n \left(\sqrt{-k^2 + \omega^2/c^2} \rho \right).$$

NOW, APPLY BOUNDARY CONDITION

$$E_{z;n}(\rho, \phi) \big|_{\rho=R} = 0, \quad \text{SO}$$

$$J_n \left(\sqrt{-k^2 + \omega^2/c^2} R \right) = J_n(k_c R) = 0,$$

$$\text{OR } k_{c;n,m} = \frac{X_{n,m}}{R},$$

WITH $X_{n,m}$ THE m th ZERO OF J_n .

WE NOW HAVE THE SHAPE OF THE TM_{mn} MODES.

LET'S FIND THE PROPAGATION PROPERTIES, WE HAVE

$$k^2 = \omega^2/c^2 - k_c^2$$

WITH CUTOFF FREQUENCY

$$\frac{\omega_{c,m,n}^2}{c^2} = k_c^2 \quad \left(= \frac{X_{m,n}^2}{R^2 c^2} \right)$$

THE PHASE VELOCITY v_g ("GUIDED")

HAS THE USUAL FORM

$$v_g = \frac{\omega}{k} = c \frac{1}{\sqrt{1 - \left(\frac{\omega_{c,m,n}}{\omega}\right)^2}}$$