



Physics 513, Electrodynamics I
Department of Physics, University of Washington
Autumn quarter 2020
December 8, 2020, 11am PST
On-line lecture

Administrative:

1. 2nd midterm exam posted this Thursday, December 10; it's due by email this Friday, December 11, 4pm PST. For exam information see the course web site.

Lecture: (a) Magnetostatics, Faraday's Law, Quasi-Static Fields. (Jackson chapter 5) (b) Maxwell's Equations, Macroscopic E&M, Conservation Laws. (Jackson chapter 6)

- 1. Comment on the vector potential and gauge transformations.**
- 2. Example: Long permeable cylindrical rod in an external B field (continued); a 2D magnetic boundary-value problem.**
- 3. Faraday' law of induction. Faraday's observation and Maxwell's extension.**
- 4. Energy in the magnetic field & self- and mutual-inductance.**

(1)

EXERCISE: POTENTIAL DESCRIBING

CONSTANT \vec{B} FIELD, SAY $\vec{B}_0 = B_0 \hat{x}$.

Since $\vec{B} = \vec{\nabla} \times \vec{A}$, \vec{A} is ORTHOGONAL
TO \vec{B}_0 . But WHICH VECTOR FOR
 \vec{A} IN THE PLANE PERPENDICULAR
TO \vec{B}_0 ?

TRY $\vec{A} = B_0 Y \hat{z} \therefore \vec{\nabla} \times \vec{A} = B_0 \hat{x}$
IT'S A VALID POTENTIAL.

TRY $\vec{A} = -B_0 Z \hat{y} \therefore \vec{\nabla} \times \vec{A} = B_0 \hat{x}$.
IT'S ALSO A VALID POTENTIAL.

CONVINCE YOURSELF A VALID POTENTIAL
CAN POINT ANYWHERE IN THE
TRANSVERSE $Y-Z$ PLANE.

How to CONNECT THE VARIOUS
VALID POTENTIALS.

Call $\vec{A}^{(Z)} = B_0 Y \hat{z}$ AND $\vec{A}^{(Y)} = -B_0 Z \hat{y}$.

LET \vec{M} BE THE VECTOR THAT
TAKES $\vec{A}^{(Z)}$ TO $\vec{A}^{(Y)}$; THAT IS

$$\begin{aligned}\vec{M} &= \vec{A}^{(Y)} - \vec{A}^{(Z)} \\ &= B_0 Y \hat{z} + B_0 Z \hat{y}.\end{aligned}$$

(2)

LET'S SEE IF \vec{M} HAS A CURL:

$\vec{\nabla} \times \vec{M} = 0$ BY TRIVIAL DIRECT CALCULATION.

APPARENTLY $\vec{A}^{(z)}$ AND $\vec{A}^{(y)}$ DIFFER BY A QUANTITY THAT HAS NO CURL. HENCE BOTH DESCRIBE THE SAME FIELD. Q.I.W.H.Y.
THE ARGUMENT CAN BE EXTENDED TO ANY VECTOR IN THE TRANSVERSE Y-Z PLANE.

SINCE $\vec{\nabla} \times \vec{M} = 0$ EVERYWHERE, IT MUST BE DESCRIbable BY A POTENTIAL Λ . THAT IS

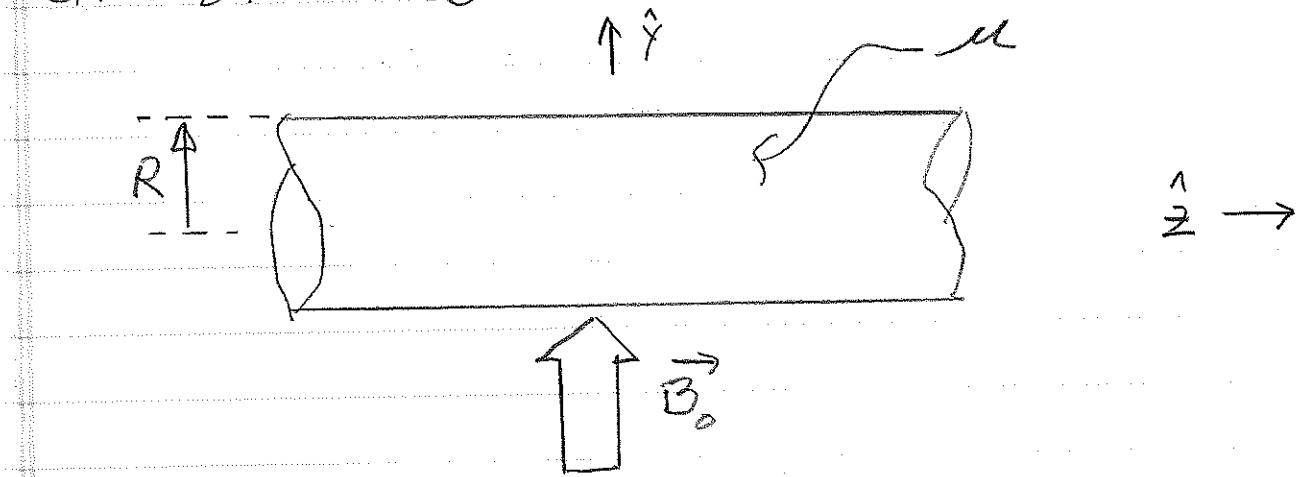
$$\vec{M} = \vec{\nabla} \Lambda.$$

THE PROCESS OF TRANSFORMING $\vec{A}^{(y)}$ TO $\vec{A}^{(z)}$ IS AN EXAMPLE OF A "GAUGE TRANSFORMATION". Λ IS THE (SCALAR) GAUGE FUNCTION.

WE'LL SEE NEXT QUARTER THAT WHEN $\vec{A} \rightarrow \vec{A}'$ BY ADDING $\vec{\nabla} \Lambda$, $\vec{\Phi}$ MUST GO TO $\vec{\Phi}'$ BY SUBTRACTING $\lambda \vec{N}$ ft.

(3)

BACK TO THE EXAMPLE: LONG PERMEABLE CIRCULAR ROD IN TRANSVERSE \vec{B} FIELD.



FIND \vec{A} EVERYWHERE.

THE SYSTEM IS TRANSLATIONALLY INVARIANT: ALL $\frac{\partial}{\partial z}$ VANISH.

$$\vec{B} = \vec{\nabla} \times \vec{A} \rightarrow B_x = \frac{\partial}{\partial y} A_z, \quad B_y = -\frac{\partial}{\partial x} A_z,$$

Q: WHAT HAPPENED TO A_z ?

A: THE SYMMETRY OF THE SYSTEM

IS SUCH THAT, THE ROD, FLIPPED END-FOR-END, IS THE SAME SYSTEM. UNDER THIS OPERATION, $B_z \rightarrow -B_z$, A DIFFERENT MAGNETIC FIELD FOR THE SAME SYSTEM. HENCE, $B_z = 0$.

OR, ARGUE FROM $\frac{\partial \vec{A}}{\partial z} = 0$.

(4)

FOR A TRANSLATIONALLY INVARIANT ("2D") SYSTEM, LAPLACE'S AND POISSON'S EQUATIONS REDUCE TO

$$\nabla^2 A_2 = 0, \quad \nabla^2 A_2 = -\mu J_2.$$

FOR THE ROD POTENTIAL, BECAUSE OF THE BOUNDARY, THERE ARE SEPARATE SOLUTIONS FOR $r > R$ AND $r < R$.

INSIDE THE ROD, THE POTENTIAL HAS FORM (C.F., LECTURE OCT. 22 OR JACKSON E&M'S. 2.69);

$$A_2(r < R) = \sum_l (a_l \cos l\theta + b_l \sin l\theta) r^l.$$

Q: WHY ARE r^{-l} TERMS ABSENT?

A: WE EXPECT A_2 TO BE NON-SINGULAR FOR $r \rightarrow 0$.

5

OUTSIDE THE ROD: AT LARGE r THE POTENTIAL SHOULD APPROACH THAT FOR A CONSTANT \vec{B} FIELD, THAT IS,

$$A_2 = B_0 Y \quad (= B_0 r \sin\theta).$$

Q: WHY IS A_2 IN THIS FORM?

A: $\vec{B} = \vec{\nabla} \times \vec{A} = \frac{\partial A_2}{\partial \theta} \hat{x} = \vec{B}_0$.

THE OUTSIDE SOLUTION THEREFORE HAS FORM

$$A_2(r > R) = B_0 r \sin\theta$$

$$+ \sum_l (c_l \cos l\theta + d_l \sin l\theta) r^{-l}.$$

Q: WHY ARE r^l TERMS ABSENT?

A: WE'D LIKE THE POTENTIAL TO APPROXIMATE $B_0 Y \approx B_0 r \sin\theta$ FOR r LARGE WHETHER OR NOT THE ROD IS THERE.

Q: COULD WE HAVE FOUND $A_2(r > R)$ HAS TERM $B_0 r \sin\theta$ BY KEEPING THE $l=1$ r^l TERMS?

A: YES.

(6)

APPLY MAGNETIC BOUNDARY CONDITIONS,

- $\vec{\nabla} \cdot \vec{B} = 0$; $\vec{B} \cdot \hat{n}$ IS CONTINUOUS ACROSS THE $r=R$ SURFACE.

RECALL THIS IMPLIED THE MAGNETIC FLUX CROSSING THE SURFACE IS CONTINUOUS. FOR ANY CLOSED LOOP EMBEDDED IN THE SURFACE

$\oint \vec{A} \cdot d\vec{l}$ ($= \Phi_m$) IS CONTINUOUS ACROSS THE BOUNDARY. IF YOU CONSIDER A THIN RECTANGULAR LOOP EMBEDDED IN THE SURFACE, WITH LONG DIRECTION ALONG \hat{z} :

$$A_{z_{in}} \Big|_{r=R} = A_{z_{out}} \Big|_{r=R}$$

WE JUST REDUCED A BOUNDARY CONDITION ON \vec{A} FROM LAST LECTURE, HERE APPLIED SPECIFICALLY TO A TRANSLATIONALLY-INVARIANT SYSTEM.

• $\vec{\nabla} \times \vec{H} = \vec{J}_{\text{TRUE}}$: For no true surface currents,

$$\hat{n} \times \left(\frac{\vec{B}(r < R)}{\mu} \Big|_{r=R} - \frac{\vec{B}(r > R)}{\mu_0} \Big|_{r=R} \right) = 0,$$

(SEE LAST LECTURE OR
JACKSON EQN. 5.87.)

THAT IS, THE TRANSVERSE
(PARALLEL,) PERP COMPONENT COMPONENT
OF \vec{H} IS CONTINUOUS ACROSS
THE $r = R$ SURFACE, HENCE

$$\frac{1}{\mu} \frac{d}{dr} A_z(r < R) \Big|_{r=R} = \frac{1}{\mu_0} \frac{d}{dr} A(r > R) \Big|_{r=R},$$

Q: How did the boundary condition reduce to this form?

A: $\hat{n} \times \frac{\vec{B}(r < R)}{\mu} \Big|_{r=R}$ is the

PARALLEL component of \vec{H} at $r=R$
(ROTATED 90° IN THE SURFACE).

THAT IS

$$\frac{\vec{B}(r < R)}{\mu} \Big|_{r=R} = \frac{\vec{B}(r > R)}{\mu_0} \Big|_{r=R},$$

(8)

$$\vec{B}(r < R) \Big|_{r=R} = \vec{\nabla} \times \vec{A}(r < R) \Big|_{r=R},$$

But $\vec{A} \sim \hat{z}$, so

$$\vec{\nabla} \times \vec{A} = \frac{1}{\mu} \frac{dA_z}{dr} \hat{r} - \frac{dA_z}{dr} \hat{\phi}.$$

WE'RE ONLY INTERESTED IN
THE PARALLEL COMPONENT ϕ ,
NOT THE NORMAL COMPONENT \hat{r} .
HENCE

$$\frac{1}{\mu} \frac{dA_z}{dr} \Big|_{r=R} = \frac{1}{\mu_0} \frac{d}{dr} A_z(r > R) \Big|_{r=R}$$

AT THIS POINT THE STRUCTURE
OF THE EQUATIONS IS THE SAME
AS THAT OF THE DIELECTRIC
ROD IN A TRANSVERSE \vec{E} FIELD.
ONLY $\ell=ll$ TERMS REMAIN AND

$$A_z(r < R) = \frac{2\mu}{\mu + \mu_0} B_0 r \sin\theta$$

$$A_z(r > R) = \left(1 + \frac{\mu - \mu_0}{\mu + \mu_0} \left(\frac{R}{r}\right)^2\right) B_0 r \sin\theta,$$

(9)

THE INSIDE POTENTIAL IN RECTANGULAR COORDINATES IS

$$A_2(r < R) = \frac{2\mu}{\mu + \mu_0} B_0 Y,$$

WITH A MAGNETIC $\vec{B} = \vec{\nabla} \times \vec{A}$ FIELD

$$\vec{B}(r < R) = \frac{2\mu}{\mu + \mu_0} B_0 \hat{Y},$$

THIS IS A CONSTANT INNER FIELD
ANOTHER WAY TO WRITE THIS IS:

$$\vec{B}(r < R) = \frac{\mu - \mu_0}{\mu + \mu_0} B_0 \hat{X} + B_0 \hat{Y},$$

THE INDUCED (AS OPPOSED TO THE ROTATIONAL OR EXTERNAL FIELD) IS

$$\frac{\mu - \mu_0}{\mu + \mu_0} B_0 \hat{X}.$$

THE INDUCED FIELD IS IN THE SAME DIRECTION AS B_0 .

NOTICE HOW

DIFFERENT THIS IS COMPARED TO
THE POLARIZATION OF DIELECTRICS
IN AN EXTERNAL E-FIELD

(10)

THE OUTSIDE FIELD IS

$$\vec{B}(r>R) = \nabla \times \vec{A}(r>R)$$

RECALL $\vec{A} \sim \hat{z}$, so

$$\vec{B}(r>R) = B_0 \hat{x} + \frac{\mu - \mu_0}{\mu + \mu_0} B_0 \frac{R^2}{r^2} \left\{ \cos \theta \hat{r} + \sin \theta \hat{\phi} \right\}$$

WE'VE SEEN SUCH A CHARACTER OF FIELDS BEFORE FOR THE DIELECTRIC ROD IN AN EXTERNAL \vec{E} FIELD.

THE FIRST TERM IS THE EXTERNAL, CONSTANT \vec{B} FIELD.

THE SECOND TERM IS THE 2D DIPOLE FIELD. (LECTURE OCT. 27, P. 21)

FARADAY'S LAW OF INDUCTION.

RECALL IN ELECTROSTATICS $\vec{\nabla} \times \vec{E} = 0$.

ALSO RECALL, TO SUPPORT STATIONARY CURRENTS THERE MUST BE ELECTRIC FIELDS FOR WHICH $\vec{\nabla} \times \vec{E} \neq 0$.

IT WAS OBSERVED THAT AN ELECTRIC FIELD FOR WHICH $\vec{\nabla} \times \vec{E} \neq 0$ ACCOMPANIES A TIME-VARYING MAGNETIC FIELD. MORE PRECISELY (FOR MAGNETIC FLUX Φ_M):

IN A CIRCUIT

$$-IR + \mathcal{E} = -\frac{d}{dt} \Phi_M. \text{ Faraday's Law.}$$

\mathcal{E} IS THE ELECTROMOTIVE FORCE IN THE CIRCUIT $\oint \vec{E} \cdot d\vec{l}$

AND NOTICE THE TOTAL TIME DERIVATIVE.

THIS RELATION IS IN NO WAY DERIVABLE FROM WHAT WE'VE SEEN UP TO NOW.

(It's asserted, in, e.g., GRIFFITHS, THAT FARADAY'S LAW IS A CONSEQUENCE OF CONSERVATION-OF-ENERGY APPLIED TO THE OVERALL ENERGY BALANCE OF CURRENTS IN MAGNETIC FIELDS. I'M PRETTY SURE THIS IS WRONG.)

$\frac{d}{dt} \Phi_M$ CAN HAVE CONTRIBUTIONS FROM CHANGING \vec{B} , CHANGING AREA OF CIRCUIT IN $\Phi_M = \iint \vec{B} \cdot \hat{n} da$, OR MOTION OF THE CIRCUIT.

MAXWELL VERY MUCH APPRECIATED THE SIGNIFICANCE OF FARADAY'S OBSERVATION, BUT MAXWELL WANTED TO CONSIDER A LOOP WITHOUT A WIRE. TO DO SO, MAXWELL NOTED THAT THE TANGENTIAL (PARALLEL) E -FIELD IS CONTINUOUS ACROSS THE WIRE, SO THE EXPRESSION $-IR + E = -\frac{d}{dt} \Phi_M$ AS WECC APPLIES TO THE REGION ADJACENT TO THE WIRE.

(13)

MAXWELL THEN NOTED ALL THE PHYSICAL CHARACTERISTICS OF THE WIRE (e.g., R) ARE EMBEDDED IN THE IR TERM, NOT THE $\oint \vec{E} \cdot d\vec{l}$ TERM. HENCE THE RELATION DOES NOT DEPEND ON THERE BEING A CURRENT-CARRYING CONDUCTOR AND

$$\mathcal{E} = -\frac{d}{dt} \Phi_M$$

IS A GENERAL PHYSICAL LAW REGARDING THE \vec{E} FIELD IN VACUUM TO A CHANGING \vec{B} -FIELD. THAT IS

$$\oint \vec{E} \cdot d\vec{l} = -\frac{d}{dt} \iint \vec{B} \cdot \hat{n} da$$

$$\iint \vec{\nabla} \times \vec{E} \cdot \hat{n} da = -\frac{d}{dt} \iint \vec{B} \cdot \hat{n} da$$

FOR ANY SURFACE CONNECTED TO THE LOOP.

IF THE MEDIA IS STATIONARY

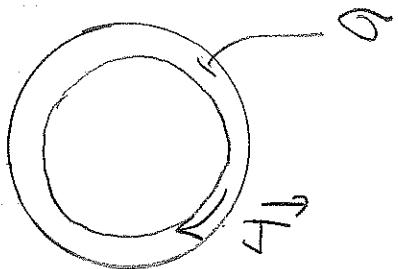
$$\frac{d}{dt} \rightarrow \frac{d}{dt} \text{ AND}$$

$$\vec{\nabla} \times \vec{E} = -\frac{d}{dt} \vec{B} \text{ IS A LAW OF NATURE.}$$

FARADAY'S LAW.

(14)

TRIVIAL EXAMPLE: CIRCULAR LOOP
CARRYING CURRENT.

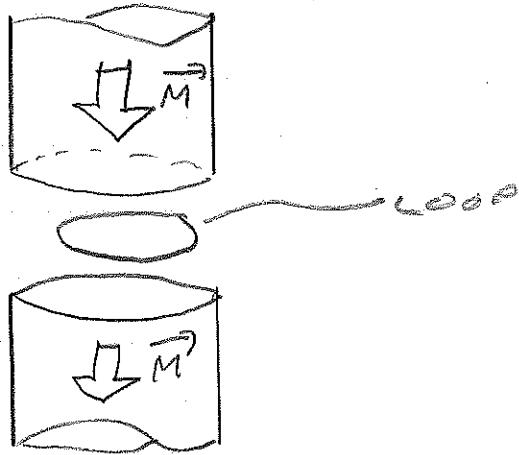


$\vec{J} = \sigma \vec{E}$, so, obviously

$\oint \vec{E} \cdot d\vec{l} \neq 0$. \vec{E} HAS A

CURL SOMEWHERE,

How would you produce such a current? By, e.g., PUTTING THE LOOP BETWEEN THE POLES OF AN ELECTROMAGNETIC AND VARYING THE APPLIED FREQUENCY



(13)

HERE $\frac{d\vec{B}}{dt} \neq 0$ THOUGH THE LOOP.

SO $\oint \vec{E} \cdot d\vec{l} \neq 0$ AROUND

THE LOOP AND CURRENT FLOWS.

NOTICE IT DOESN'T MAKE PHYSICAL SENSE TO SAY THE \vec{E} WAS PRODUCED AT A PARTICULAR PLACE IN THE CIRCUIT.

OUR MAXWELL EQUATIONS SO FAR

$$\vec{\nabla} \cdot \vec{E} = \frac{1}{\epsilon_0}; \quad \vec{\nabla} \cdot \vec{B} = 0,$$

$$\vec{\nabla} \times \vec{E} + \frac{d\vec{B}}{dt} = 0; \quad \vec{\nabla} \times \vec{B} = \mu_0 \vec{J}$$

THIS WILL NEED MODIFICATION.

Q: GUESS HOW YOU'D MODIFY

$\vec{\nabla} \times \vec{E} + \frac{d\vec{B}}{dt}$ TO ACCOUNT FOR MOVING MEDIA?

A: Hint: CONSIDER

$$\vec{F} = \epsilon \vec{E} + \mu \vec{B},$$

ENERGY REATIONS IN QUASI-STATIONARY ($v \ll c$) MOTION AND FIELD ($\frac{d\vec{D}}{dt} \ll J$): CURRENT-CARRYING SYSTEMS.

CONSIDER A BATTERY (A "SOURCE" OF E) DRIVING CURRENTS. THERE'S HEATING AND A \vec{B} FIELD DUE TO CURRENTS.

RECALL $\vec{J} = \sigma(\vec{E}^I + \vec{E}^R)$
WITH \vec{E}^I AND \vec{E}^R IRROTATIONAL (CURL-LESS) AND ROTATIONAL (NON-ZERO CURL) FIELDS.

WE THEREFORE HAVE

$$\vec{J} \cdot \vec{J} = \sigma(\vec{E}^I \cdot \vec{J} + \vec{E}^R \cdot \vec{J}), \text{ or}$$

$$\vec{E}^R \cdot \vec{J} = \frac{\vec{J}^2}{\sigma} - \vec{E}^I \cdot \vec{J}.$$

THE $\vec{E}^R \cdot \vec{J}$ (AS WE SAW BEFORE) HAS UNITS OF POWER/VOLUME: THE ROTATIONAL FIELDS ARE SUPPLIED BY THE BATTERY. SO $\vec{E}^R \cdot \vec{J}$ IS THE TIME RATE PER VOLUME OF WORK DONE BY THE BATTERY.

(17)

WE'VE SEEN $\frac{J^2}{\sigma}$ IN UNDERGRADUATE ELECTRODYNAMICS, IT'S SOURCE HEATING.

THE REMAINING TERM $- \vec{E}^I \cdot \vec{J}$ THEREFORE SEEKS TO BE THE TIME RATE PER VOLUME OF ENERGY FEEDING THE MAGNETIC FIELD.

Q: WHY CAN WE NEGLECT THE DISPLACEMENT CURRENT IN \vec{J} ?

Now, INTEGRATE THE LOCAL ENERGY BALANCE FROM THE PREVIOUS PAGE OVER ALL SPACE.

$$\text{FOR } \vec{\partial} \times \vec{H} = \vec{J},$$

$$\iiint \vec{E}^R \cdot (\vec{\nabla} \times \vec{H}) dV$$

$$= \iiint \frac{(\vec{\nabla} \times \vec{H})^2}{\sigma} dV - \iiint \vec{E}^I \cdot (\vec{\nabla} \times \vec{H}) dV$$

(18)

STUDY THE LAST TERM $\iiint \vec{E}^I \cdot (\vec{\nabla} \times \vec{H}) dV$.

IT LOOKS LIKE PART OF

$$\vec{\nabla} \cdot (\vec{E}^I \times \vec{H}) = \vec{H} \cdot (\vec{\nabla} \times \vec{E}^I) + \vec{E}^I \cdot (\vec{\nabla} \times \vec{H}).$$

HOWEVER $\iiint \vec{\nabla} \cdot (\vec{E}^I \times \vec{H}) dV$

$$= \iint \vec{E}^I \times \vec{H} \cdot \hat{n} d\Omega \rightarrow 0$$

FOR LOCATED SOURCES.

COMMENT: WE'LL NEED TO BE MORE CAREFUL LATER WHEN WE CONSIDER RADIATION.

FINALLY. BECAUSE $\vec{\nabla} \times \vec{E} = -\frac{d}{dt} \vec{B}$,
HENCE

$$\iiint \vec{E}^I \cdot (\vec{\nabla} \times \vec{H}) dV$$

$$= \iiint \frac{(\vec{\nabla} \times \vec{H})^2}{c} dV + \iiint \vec{H} \cdot \frac{d}{dt} \vec{B} dV.$$

THE LAST TERM IS CLEARLY THE RATE PER VOLUME ENERGY IS FEEDING THE MAGNETIC FIELD, THAT IS, WE IDENTIFY THE MAGNETIC FIELD FREE-ENERGY

$$SU_M = \iiint \vec{H} \cdot S \vec{B} dV,$$

(19)

NOTICE THE SLIGHT DIFFERENCE
AS COMPARED TO THE
ELECTRIC FREE ENERGY

$$\delta U_E = \iiint \vec{E} \cdot \delta \vec{D} \, dv,$$

JUST LIKE FOR LINEAR DIELECTRICS
WE FOUND THIS FORM OF δU_E
LED TO FREE ENERGY

$$U_E = \frac{1}{2} \iiint \vec{E} \cdot \vec{D} \, dv,$$

FOR PERMEABLE MEDIA $\vec{B} = \mu \vec{H}$,

$$U_M = \frac{1}{2} \iiint \vec{B} \cdot \vec{H} \, dv.$$

THIS IS ENERGY IN TERMS OF
FIELDS. WHAT ABOUT ENERGY
IN TERMS OF SOURCES AND POTENTIALS?

In U_M RECALL $\vec{B} = \vec{\nabla} \times \vec{A}$.

FURTHER RECALL

$$\vec{\nabla} \cdot (\vec{A} \times \vec{H}) = \vec{H} \cdot (\vec{\nabla} \times \vec{A}) - \vec{A} \cdot (\vec{\nabla} \times \vec{H}).$$

Q: WHY DOES THE TOTAL OVERAGE
VANISH?

(20)

$$\text{HENCE } U_M = \frac{1}{2} \iiint \vec{A} \cdot (\vec{P} + \vec{H}) dV \quad \text{or}$$

$$U_M = \frac{1}{2} \iiint \vec{A} \cdot \vec{J} dV.$$

Q: Can you have guessed this form of U_M ?

A: Hint: Recall $U_E = \frac{1}{2} \iiint \epsilon \rho dV$.

RECALL FROM ELECTROSTATICS:
 THE FACTOR OF 1/2 TAKES
 INTO ACCOUNT THAT THE
 POTENTIALS (Φ AND \vec{A}) INCLUDE
 THE FIELDS OF THE SOURCES
 (P , J) THEMSELVES.

YOU MIGHT WANT TO ASK WHAT
 THE INTERACTION ENERGY IS OF
 SOURCES IN EXTERNAL FIELDS. IN
 THIS CASE

$$U = \iiint \vec{J} \cdot \vec{A}_{\text{EXT}} dV + \iiint \vec{A} \cdot \vec{\Phi}_{\text{EXT}} dV.$$