

SPECIAL LECTURE

VOLUME FORCES IN DIELECTRICS

ADAPTED FROM STRATTON "ELECTROMAGNETIC THEORY" : CHAPT II

RECALL, THE (FREE) ENERGY IN THE PRESENCE OF DIELECTRICS IS

$$U = \frac{1}{2} \iiint \vec{E} \cdot \vec{D} \, dV \quad (\text{JACKSON EQN 4.89})$$

WE FOUND THIS IN LECTURE BY STUDYING A "VIRTUAL" PROCESS IN WHICH FREE CHARGES WE SLOWLY ADDED TO A SYSTEM, NOT ALLOWING BOUNDARIES TO MOVE (THEREBY ENSURING NO MECHANICAL WORK IS DONE BY MECHANICAL MOTIONS).

WE'LL NOW CONSIDER A DIFFERENT "VIRTUAL" PROCESS: THE POSITIONS OF CHARGES AND DIELECTRIC MATERIAL ARE "VIRTUALLY" DISPLACED A DISTANCE  $\delta \vec{r}$  AT EVERY POINT IN THE SYSTEM, BUT WE DONT ADD FREE CHARGES,

A SUBTLETY: IN THIS LATER PROCESS, IS  $U = \frac{1}{2} \iiint \vec{E} \cdot \vec{D} \, dV$  STILL VALID? A LONG DISCUSSION LEADS TO "YES", BASED ON THE FIELDS BEING CONSERVATIVE.

IN THIS "VIRTUAL" DISPLACEMENT, THE (FREE) ENERGY CHANGES BY

$$\delta U = - \iiint \vec{F} \cdot \delta \vec{r} \, dV,$$

WHERE  $\vec{F}$  IS THE "VOLUME FORCE"  $\frac{dF}{dV}$

A SUBLETY: THE "VIRTUAL VELOCITIES"  $\vec{v}$  DUE TO THE VIRTUAL DISPLACEMENTS ARE SO LOW THAT THE DISPLACEMENT PROCESS IS REVERSIBLE AND ISOTHERMAL. HENCE, THE CHANGE IN (FREE) ENERGY IS THE MECHANICAL WORK.

IT IMMEDIATELY FOLLOWS THAT

$$\frac{dU}{dt} = - \iiint \vec{F} \cdot \vec{v} \, dV$$

THE VIRTUAL DISPLACEMENTS CAN CHANGE HOW CHARGE  $\rho$  IS DISTRIBUTED (LEADING TO  $\delta \rho$ ) AND A CHANGE IN THE DIELECTRIC CONSTANT  $\epsilon$  (MATERIAL MOVES). THE RESULTING (FREE) ENERGY CHANGE IS

$$\begin{aligned} \delta U &= \delta \left[ \frac{1}{2} \iiint \vec{E} \cdot \vec{D} \, dV \right] \\ &= \frac{1}{2} \iiint D^2 \left( \frac{1}{\epsilon} \right) \delta \epsilon \, dV + \iiint \vec{E} \cdot \delta \vec{D} \, dV \\ &= -\frac{1}{2} \iiint E^2 \delta \epsilon \, dV + \iiint \vec{E} \cdot \delta \vec{D} \, dV \end{aligned}$$

THE FIRST TERM IS THE (FREE) ENERGY CHANGE DUE TO THE CHANGE IN THE DIELECTRIC CONSTANT INDUCED BY THE VIRTUAL DISPLACEMENT.

RECALL THE (INTEGRATION BY PARTS) IDENTITY  $\vec{\nabla} \cdot (\Phi \vec{A}) = \Phi \vec{\nabla} \cdot \vec{A} + \vec{A} \cdot \vec{\nabla} \Phi$ , APPLIED TO THE SECOND TERM:

$$\iiint \vec{E} \cdot \delta \vec{D} \, dV = - \iiint \vec{\nabla} \Phi \cdot \delta \vec{D} = \iiint \Phi \vec{\nabla} \cdot \delta \vec{D} \, dV$$

(WHERE GAUSS'S LAW ALLOWS US TO

IGNORE THE TOTAL DIVERGENCE),  $\oint$

$$\iiint \vec{E} \cdot \delta \vec{D} \, dV = \iiint \Phi \delta \rho \, dV$$

WE THUS HAVE

$$\frac{dU}{dt} = \iiint \left\{ \Phi \frac{d\rho}{dt} - \frac{1}{2} \epsilon^2 \frac{d\epsilon}{dt} \right\} dV$$

WE'D LIKE TO SOMEHOW EXPRESS THIS IN TERMS OF  $\vec{F}$ . TO THIS END, WE RECALL CONSERVATION FOR CHARGE  $\rho$  AND MASS  $\rho_m$ :

$$\vec{\nabla} \cdot \rho \vec{v} + \frac{d\rho}{dt} = 0; \quad \vec{\nabla} \cdot \rho_m \vec{v} + \frac{d\rho_m}{dt} = 0.$$

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THIS IS A GOOD PLACE TO INTRODUCE THE "CONNECTIVE DERIVATIVE", THIS IS THE TOTAL DERIVATIVE OF A CERTAIN THING EVALUATED SO THE OBSERVATION POINT FOR THE DERIVATIVE IS CO-MOVING WITH THE VELOCITY FLOW, WE WRITE THIS AS  $\frac{D}{Dt}$ .

FOR EXAMPLE, THE CONNECTIVE DERIVATIVE OF THE DIELECTRIC CONSTANT IS

$$\begin{aligned}\frac{D\epsilon}{Dt} &= \frac{\partial \epsilon}{\partial t} + \frac{\partial \epsilon}{\partial x} \frac{dx}{dt} + \frac{\partial \epsilon}{\partial y} \frac{dy}{dt} + \frac{\partial \epsilon}{\partial z} \frac{dz}{dt} \\ &= \frac{\partial \epsilon}{\partial t} + \vec{v} \cdot \vec{\nabla} \epsilon\end{aligned}$$

FOR CHARGE  $\rho$  AND DIELECTRIC CONSTANT  $\epsilon$ , WE THEN HAVE

$$\frac{D\rho_m}{Dt} = \frac{\partial \rho_m}{\partial t} - \vec{v} \cdot \vec{\nabla} \rho_m$$

$$\frac{D\epsilon}{Dt} = \frac{\partial \epsilon}{\partial t} - \vec{v} \cdot \vec{\nabla} \epsilon$$

SUBJECT: WE ASSUME THE DEPENDENCE OF THE DIELECTRIC CONSTANT  $\epsilon$  ON MASS DENSITY  $\rho_m$  IS KNOWN, EITHER THROUGH THEORY OR EMPIRICALLY.

THAT IS, WE HAVE  $\frac{DE}{Dt} = \frac{dE}{d\rho_m} \frac{D\rho_m}{Dt}$ ,  
WITH  $dE/d\rho_m$  KNOWN,

BY THE WAY, THE CLAUSIUS -  
MOSOTTI FORM SPECIAL LECTURE I  
IS A GOOD ESTIMATE OF  $dE/d\rho_m$ ,

SUBTIETY: ASSUMING  $E$  HAS NO  
TEMPERATURE DEPENDENCE WORKS  
IN GENERAL ONLY IF THE VIRTUAL  
PROCESS IS ISOTHERMAL.

INSERTING THE CONSERVATION EQUATIONS  
INTO THE EXPRESSION FOR  $DE/dt$   
ABOVE GIVES

$$\frac{DE}{Dt} = \frac{dE}{d\rho_m} \left\{ \frac{d\rho_m}{dt} + \vec{v} \cdot \vec{\nabla} \rho_m \right\}$$

$$= \frac{dE}{d\rho_m} \left\{ \vec{v} \cdot \vec{\nabla} \rho_m - \vec{\nabla} \cdot \rho_m \vec{v} \right\}$$

$$= \frac{dE}{d\rho_m} \rho_m \vec{\nabla} \cdot \vec{v}$$

WE THUS HAVE

$$\frac{dE}{dt} = - \frac{dE}{d\rho_m} \rho_m \vec{\nabla} \cdot \vec{v} - \vec{v} \cdot \vec{\nabla} E$$

WE THEN HAVE THE EXPRESSION FOR  $dU/dt$  ON PAGE 3 IN THE FORM

$$\frac{dU}{dt} = \iiint \left\{ \underbrace{-\Phi \nabla \cdot \rho \vec{V}}_{(1)} + \underbrace{\frac{1}{2} E^2 \frac{d\epsilon}{d\rho_m}}_{(2)} \nabla \cdot \vec{V} \right. \\ \left. + \underbrace{\vec{V} \cdot \left( \frac{1}{2} E^2 \nabla \epsilon \right)}_{(3)} \right\}$$

WE'RE ALMOST DONE. TO FIND THE VOLUME FORCE  $\vec{F}$ , WE NEED TO WRITE THE INTEGRAND AS A DOT PRODUCT OF "SOMETHING"  $\cdot \vec{V}$ . WE CAN THEN IDENTIFY "SOMETHING" AS THE VOLUME FORCE.

TERM 1 HAS APPLIED THE IDENTITY  $\nabla \cdot (\Phi \vec{A}) = \Phi \nabla \cdot \vec{A} + \vec{A} \cdot \nabla \Phi$ , GAUSS'S LAW, WITH A SURFACE COMPLETELY OUTSIDE THE SYSTEM. THIS GIVES

$$\iiint \Phi \nabla \cdot (\rho \vec{V}) dV = - \iiint \rho \nabla \Phi \cdot \vec{V} dV$$

TERM 2 IS SIMILAR, AGAIN ELIMINATING THE SURFACE TERM:

$$\frac{1}{2} \iiint E^2 \rho_m \frac{d\epsilon}{d\rho_m} \nabla \cdot \vec{V} dV \\ = - \frac{1}{2} \iiint \nabla \cdot \left( E^2 \frac{d\epsilon}{d\rho_m} \rho_m \right) \cdot \vec{V} dV$$



COMBINED, THESE GIVE

$$\frac{dU}{dt} = \iiint \left\{ -\rho \vec{E} + \frac{1}{2} E^2 \vec{\nabla} \epsilon - \frac{1}{2} \vec{\nabla} \left( E^2 \frac{d\epsilon}{d\rho_m} \rho_m \right) \right\} \cdot \vec{V} dV$$

THE "SOMETHING" IN BRACKETS IS THE VOLUME FORCE:

$$\vec{F} = \underbrace{\rho \vec{E}}_{(1)} - \underbrace{\frac{1}{2} E^2 \vec{\nabla} \epsilon}_{(2)} + \underbrace{\frac{1}{2} \vec{\nabla} \left( E^2 \frac{d\epsilon}{d\rho_m} \rho_m \right)}_{(3)}$$

TERM 1 IS THE USUAL VOLUME FORCE

$$\vec{F} = \rho \vec{E} \left\{ = (\vec{\nabla} \cdot \vec{J}) \vec{E} \right\}$$

TERM 2 ARISES FROM AN INHOMOGENEOUS DIELECTRIC ( $\vec{\nabla} \epsilon \neq 0$ ) IN AN ELECTRIC FIELD,

TERM 3 IS USUALLY IGNORED, THE EFFECT IS CALLED "ELECTRORETRACTION" AN IT ARISES FROM A DENSITY - DEPENDENT DIELECTRIC IN AN INHOMOGENEOUS ELECTRIC FIELD, NOTICE THIS TERM IS A PURE GRADIENT, SO IF THE VOLUME IS LARGE ENOUGH (TO BE OUTSIDE THE FIELD) ITS INTEGRAL GIVES NO NET FORCE, THAT'S WHY THIS TERM IS OFTEN IGNORED,

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SUBTLETY: IGNORING THE ELECTROSTRICTION  
IN A LARGE ENOUGH VOLUME INDEED  
GIVES THE CORRECT TOTAL BULK FORCE,  
BUT THE INCORRECT PRESSURE AT  
POINTS WITHIN THE DIELECTRIC