Astr 509: Astrophysics III: Stellar Dynamics Winter Quarter 2005, University of Washington, Željko Ivezić

Lecture 8: Equilibria of Collisionless Systems. II

The Jeans Equations

The collisonless Boltzmann Equation

$$\frac{\partial f}{\partial t} + \sum_{i=1}^{3} \left[v_i \frac{\partial f}{\partial x_i} - \frac{\partial \Phi}{\partial x_i} \frac{\partial f}{\partial v_i} \right] = 0$$
(1)

or

$$\frac{\partial f}{\partial t} + \mathbf{v}\nabla f = \nabla \Phi \frac{\partial f}{\partial \mathbf{v}}$$
(2)

where

$$f \equiv f(\mathbf{x}, \mathbf{v}) \tag{3}$$

Introduce the summing convention, so that

$$\frac{\partial f}{\partial t} + v_i \frac{\partial f}{\partial x_i} - \frac{\partial \Phi}{\partial x_i} \frac{\partial f}{\partial v_i} = 0$$
(4)

Now let us integrate the CBE expressed in form (4) over all velocities:

$$\int \frac{\partial f}{\partial t} d^3 \mathbf{v} + \int v_i \frac{\partial f}{\partial x_i} d^3 \mathbf{v} - \frac{\partial \Phi}{\partial x_i} \int \frac{\partial f}{\partial v_i} d^3 \mathbf{v} = 0.$$
 (5)

How do we evaluate these integrals? Two rules:

- 1. Derivative wrt $\mathbf{x},$ or a function of $\mathbf{x},$ can be taken out
- 2. Introduce notation

$$\int g(\mathbf{v}) f \mathrm{d}^3 \mathbf{v} = \langle g \rangle \int f \mathrm{d}^3 \mathbf{v} \tag{6}$$

where

$$\nu(\mathbf{x}) = \int f d^3 \mathbf{v} \tag{7}$$

is the number density as a function of position.

Then $\int \frac{\partial f}{\partial t} d^{3}\mathbf{v} + \int v_{i} \frac{\partial f}{\partial x_{i}} d^{3}\mathbf{v} - \frac{\partial \Phi}{\partial x_{i}} \int \frac{\partial f}{\partial v_{i}} d^{3}\mathbf{v} = 0.$ (8)

with

$$\overline{v}_i \equiv \frac{1}{\nu} \int f v_i \mathrm{d}^3 \mathbf{v},\tag{9}$$

becomes

$$\frac{\partial \nu}{\partial t} + \frac{\partial (\nu \overline{\nu}_i)}{\partial x_i} = 0.$$
 (10)

This is just the continuity equation for the stellar number density in real space.

More interesting results are obtained by multiplying the CBE with higher powers of $\mathbf{v}.$

E.g. take the first velocity moment of the CBE. Then

$$\int \frac{\partial f}{\partial t} d^3 \mathbf{v} + \int v_i \frac{\partial f}{\partial x_i} d^3 \mathbf{v} - \frac{\partial \Phi}{\partial x_i} \int \frac{\partial f}{\partial v_i} d^3 \mathbf{v} = 0.$$
(11)

becomes

$$\frac{\partial}{\partial t} \int f v_j \mathrm{d}^3 \mathbf{v} + \int v_i v_j \frac{\partial f}{\partial x_i} \mathrm{d}^3 \mathbf{v} - \frac{\partial \Phi}{\partial x_i} \int v_j \frac{\partial f}{\partial v_i} \mathrm{d}^3 \mathbf{v} = 0.$$
(12)

We can use the divergence theorem to manipulate the last term

$$\int v_j \frac{\partial f}{\partial v_i} d^3 \mathbf{v} = -\int \frac{\partial v_j}{\partial v_i} f d^3 \mathbf{v} = -\int \delta_{ij} f d^3 \mathbf{v} = -\delta_{ij} \nu, \qquad (13)$$

Note that

$$v_j \frac{\partial f}{\partial v_i} = -f \frac{\partial v_j}{\partial v_i} + \frac{\partial (v_j f)}{\partial v_i}$$
(14)

and the last term must be 0 when the integration surface is expendend to infinity (where f must vanish).

Eq.(13) can be substituted into (12) giving

$$\frac{\partial(\nu\overline{v_j})}{\partial t} + \frac{\partial(\nu\overline{v_i}\overline{v_j})}{\partial x_i} + \nu\frac{\partial\Phi}{\partial x_j} = 0, \qquad (15)$$

where

$$\overline{v_i v_j} \equiv \frac{1}{\nu} \int v_i v_j f \mathrm{d}^3 \mathbf{v}.$$
 (16)

This is an equation of momentum conservation.

Each velocity can be expressed as a sum of the mean value (aka streaming motion) and the so-called peculiar velocity

$$v_i = \overline{v_i} + w_i \tag{17}$$

where $\overline{w_i} = 0$ by definition.

Then

$$\sigma_{ij}^2 \equiv \overline{w_i w_j} = \overline{(v_i - \overline{v}_i)(v_j - \overline{v}_j)} = \overline{v_i v_j} - \overline{v}_i \overline{v}_j.$$
(18)

At each point x the symmetric tensor σ^2 defines an ellipsoid whose principal axes run parallel to σ^2 's eigenvectors and whose semi-axes are proportional to the square roots of σ^2 's eigenvalues. This is called the **velocity ellipsoid** at x.

The Jeans Equations

The continuity equation:

$$\frac{\partial \nu}{\partial t} + \frac{\partial (\nu \overline{v}_i)}{\partial x_i} = 0.$$
 (19)

and the momentum equation

$$\nu \frac{\partial \overline{v_j}}{\partial t} + \nu \overline{v_i} \frac{\partial \overline{v_j}}{\partial x_i} = -\nu \frac{\partial \Phi}{\partial x_j} - \frac{\partial (\nu \sigma_{ij}^2)}{\partial x_i}$$
(20)

The term $-\nu \sigma_{ij}^2$ is a **stress tensor** – it describes an anisotropic pressure.

Note that the system is not closed: there is no "equation of state"! The multiplication by higher powers of v doesn't help – need an *ansatz*. In practice one assumes a particular form for σ_{ij}^2 , e.g. for isotropic velocity dispersion $\sigma_{ij}^2 = \sigma^2 \delta_{ij}$

The Jeans Equations

Specialization for an axially symmetric system:

First express the CBE in cylindrical coordinates

$$\frac{\partial f}{\partial t} + \dot{R}\frac{\partial f}{\partial R} + \dot{\phi}\frac{\partial f}{\partial \phi} + \dot{z}\frac{\partial f}{\partial z} + \dot{v}_R\frac{\partial f}{\partial v_R} + \dot{v}_\phi\frac{\partial f}{\partial v_\phi} + \dot{v}_z\frac{\partial f}{\partial v_z} = 0$$
(21)

With $\dot{R}\equiv v_R$, $\dot{\phi}\equiv v_{\phi}/R$, and $\dot{z}\equiv v_z$, and

$$\dot{v}_R = -\frac{\partial \Phi}{\partial R} + \frac{v_\phi^2}{R} \tag{22}$$

$$\dot{v}_{\phi} = -\frac{1}{R} \frac{\partial \Phi}{\partial \phi} - \frac{v_R v_{\phi}}{R}$$
(23)

$$\dot{v}_z = -\frac{\partial \Phi}{\partial z} \tag{24}$$

we get

The Jeans Equations

$$\frac{\partial f}{\partial t} + v_R \frac{\partial f}{\partial R} + v_z \frac{\partial f}{\partial z} + \left[\frac{v_{\phi}^2}{R} - \frac{\partial \Phi}{\partial R}\right] \frac{\partial f}{\partial v_R} - \frac{v_R v_{\phi}}{R} \frac{\partial f}{\partial v_{\phi}} - \frac{\partial \Phi}{\partial z} \frac{\partial f}{\partial v_z} = 0 \quad (25)$$

where it was assumed that $\partial/\partial \phi \equiv 0$.

Now we multiply by v_R , v_z and v_{ϕ} , and integrate over all velocities to get (assuming steady state)

$$\frac{\partial(\nu \overline{v_R^2})}{\partial R} + \frac{\partial \nu \overline{v_R v_z}}{\partial z} + \nu \left(\frac{\overline{v_R^2} - \overline{v_\phi^2}}{R} + \frac{\partial \Phi}{\partial R} \right) = 0,$$

$$\frac{\partial(\nu \overline{v_R v_\phi}}{\partial R} + \frac{\partial(\nu \overline{v_\phi v_z})}{\partial z} + \frac{2\nu}{R} \overline{v_\phi v_R} = 0, \quad (26)$$

$$\frac{\partial(\nu \overline{v_R v_z})}{\partial R} + \frac{\partial(\nu \overline{v_z^2})}{\partial z} + \frac{\nu \overline{v_R v_z}}{R} + \nu \frac{\partial \Phi}{\partial z} = 0.$$

Lovely! And powerful.

Some Applications of the Jeans Equations

- Asymmetric drift
- The local mass density
- The shape of local velocity ellipsoid
- Spheroidal components with isotropic velocity dispersion

Asymmetric drift

Observations indicate that stars with large $\overline{v_R^2}$ rotate more slowly:

$$\overline{v_{\phi}} = v_c - \overline{v_R^2}/D \tag{27}$$

with $D \approx 120$ km/s. This can be explained using the v_R Jeans equation.

Limit the consideration to z = 0, assume $\partial \nu / \partial z = 0$, define $\sigma_{\phi}^2 = \overline{v_{\phi}^2} - \overline{v_{\phi}}^2$, and note that $v_c^2 = R(\partial \Phi / \partial R)$, to get

$$\overline{v_{\phi}} = v_c - \frac{\overline{v_R^2}}{2v_c} \zeta, \qquad (28)$$

where

$$\zeta = \frac{\sigma_{\phi}^2}{\overline{v_R^2}} - 1 - \frac{\partial \ln(\nu \overline{v_R^2})}{\partial \ln R} - \frac{R}{\overline{v_R^2}} \frac{\partial(\overline{v_R v_z})}{\partial z}$$
(29)

Asymmetric drift

Assuming that $v_c \approx 220$ km/s, we are done if we can convince ourselves that $\zeta \approx 2v_c/D \approx 2.6$. Can we?

1. Locally
$$\overline{v_z^2}/\overline{v_R^2} \approx \sigma_\phi^2/\overline{v_R^2} \approx 0.45$$

- 2. For $(\partial \ln(\nu v_R^2) / \partial \ln R)$ assume that $\overline{v_R^2} \propto \nu$ because observations indicate that $\overline{v_z^2} \propto \nu$
- 3. $R(\partial(\overline{v_R v_z})/\partial z)/\overline{v_R^2}$ is somewhere between 0 and 0.55 this is significantly smaller than other terms

Hence, ζ does seem to be confined to a very narrow range of plausible values, and thus $v_a \equiv \overline{v_\phi} - v_c \propto \overline{v_R^2}$.