D. Bernoulli, Euler, and the Development of Fluid Mechanics

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Erik R. Tou, Pacific Lutheran University

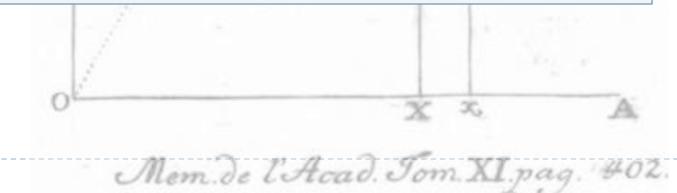
Euler Society 2014 Meeting

Mem. de l'Acad. Tom. XI.pag. 402.

Geometry vs. Analysis

"The analytical investigations of the Greek geometers are indeed models of simplicity, clearness and unrivalled elegance... some of the noblest monuments of human genius. It is a matter of deep regret, that Algebra, or the Modern Analysis, from the mechanical facility of its operations, has contributed, especially on the Continent, to vitiate the taste and destroy the proper relish for the strictness and purity so conspicuous in the ancient method of demonstration."

— John Leslie, preface to *Elements of Geometry* (1809)^[9]



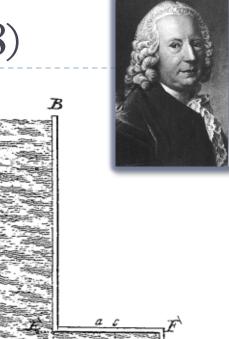
Partial Timeline of Early Fluid Mechanics

1738 [Apr/May] – Daniel Bernoulli's Hydrodynamica appears in print (first draft written c. 1733).

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TL

- 1738 [Oct] Johann Bernoulli writes to Leonhard Euler, first mentioning Hydraulica.
- 1739 [Mar/Apr] Euler receives copies of D. Bernoulli's Hydrodynamica and J. Bernoulli's Hydraulica (Part 1), nearly simultaneously.
- 1739 [May] Euler writes to each Bernoulli about their work on fluid mechanics.
- 1743 Hydraulica appears in print (in J. Bernoulli's Opera Omnia), backdated to 1732.
- ▶ **1751** Euler writes "Research on the movement of rivers" [E332], pub. 1767.
- ▶ **1752** Euler writes "Principles of the motion of fluids" [E258], pub. 1761.
- 1755 Euler writes "General principles of the motion of fluids" [E226], pub. 1757.



D. Bernoulli's Hydrodynamica (1738)

Problema.

Fig.72. S. J. Fuerit vas amplifimum A CEB (Fig. 72.) aqua conftanter plenum confervandum, tubo inftructum cylindrico & horizontali ED; fitque in extremitate tubi foramen o aquas velocitate uniformi emittens; quæritur preffio aquæ in latera tubi ED.

Solutio.

Sit altitudo fuperficiei aquez AB fupra orificium $\bullet _ a$; erit velocitas aquæ in \circ effluentis, fi prima fluxus momenta excipias, uniformis cenfenda & $\equiv \sqrt{a}$, quia vas conftanter plenum confervari affumimus; pofitaque ratione amplitudinum tubi ejusque foraminis $\equiv \frac{\pi}{i}$, erit velocitas aquæ in tubo $\equiv \frac{\sqrt{a}}{\pi}$: Si vero omne fundum FD abeffet, foret velocitas ultima aquæ in eodem tubo $\equiv \sqrt{a}$, quæ major eft quam a; lgitur aqua in tubo tendit ad majorem motum, nifus autem ejus ab appofito fundo FD impeditur: Ab hoc nifu & renifu comprimitur aqua, quæ ipfa comprefito coërcetur à lateribus

laterum proportionalem effe accelerationi feu incremento velociatis, quod aqua fit acceptura, fi in inftanti omne obstaculum motus evanescat, fic ut immediate in aërem ejiciatur.

tubi, hæcque proinde fimilent preffionem fustinent. Apparet fic preffionem

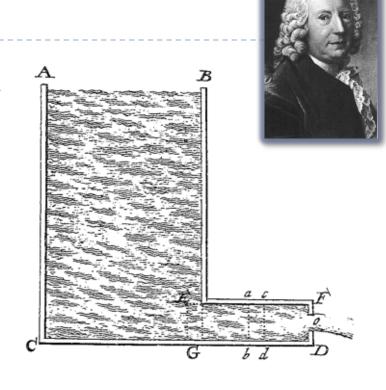
Res igitur jam eo perducta eft, ut fi durante fluxu aquæ per o, tubus E D in temporis puncto abrumpatur in cd, quæratur quantam accelerationem guttula a cbd inde fit perceptura : tantam enim prefionem fentiet particula a c in lateribus tubi fumta à præterfluente aqua : Hunc in finem confiderandum eft vas ABE cd C, atque pro eo invenienda acceleratio particulæ aqueæ efflutini proximæ, fi hæc habuerit velocitatem $\frac{\sqrt{a}}{n}$: Istud negotium fecimus generalissime in paragrapho tertis fect. V. Attamen quia in hoc cafu particulari brevis eft calculus, motum in vase decurtato ABE cd C hic iterum calculo fubducemus. Sit velocitas aquæ in tubo Ed, quæ nunc ut variabilis confideranda eft. =v: amplitudo tubi ut antea =n, longitudo Ec = c: indicetur longitudo ac particulæ aquææ infinite parvæ & effluxui proxime per dx: Erit guttula æqualis in E tubum ingreffura eodem temporis puncto quo altera acdb ejicitur: dum autom guttula in E, cujus maffa = ndx, tubum ingreditur acquirit velocitatem v, atque vim vivam nvvdx, quæ vis viva tota fait de novo generata; nullum enim, ob amplitudinem vafis A E infinitam, motum guttula in E habuit tubum nondum ingreffa: huic vi viva nvvdx addendum eft incrementum vis viva, quod aqua in Eb accipit, dum guttula ad effluit, nempe 2n cvdv: aggregatum debetur defcenfui atimali guttulæ ndx per altitudinem BE feu a: habetur igitur nvvdx + 2ncvdv = nadx

five $\frac{\sigma d\sigma}{dx} = \frac{a - \sigma \sigma}{2c}$.

 \mathbf{A}

Bernoulli's Geometry

Let the height of the surface of the water *AB* above the hole o = a; the velocity of the water flowing out at o, if the first moment of flow be excepted, is to be regarded as uniform and $= \sqrt{a}$, since we assume the vessel to be kept constantly full. Let the ratio of the width of the tube to that of the hole be n/1; then the velocity of the water in the tube $= \sqrt{a/n}$...



... the problem is now changed into this: if during the flow of the water through o the tube ED were broken at cd at an instant, one seeks the magnitude of the acceleration the volume element acbd would thence be about to obtain...

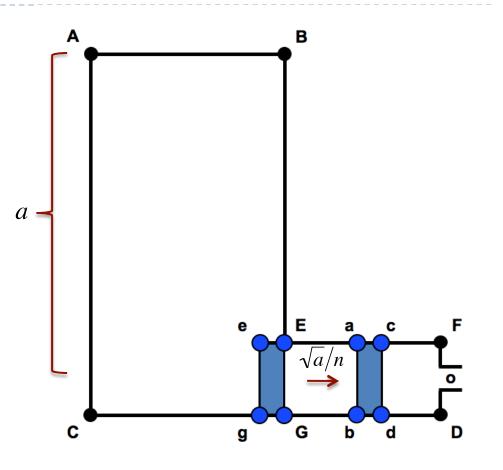
Bernoulli's Geometry

a = distance from surface AB to hole o

n =ratio of FD to o (FD is n times the width of the hole)

Aqueous particles at acbd (midway through tube) and eEGg (about to enter tube).

Velocity of water in tube is \sqrt{a}/n .



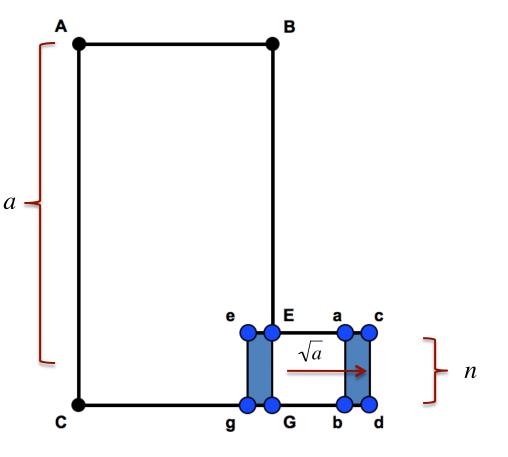
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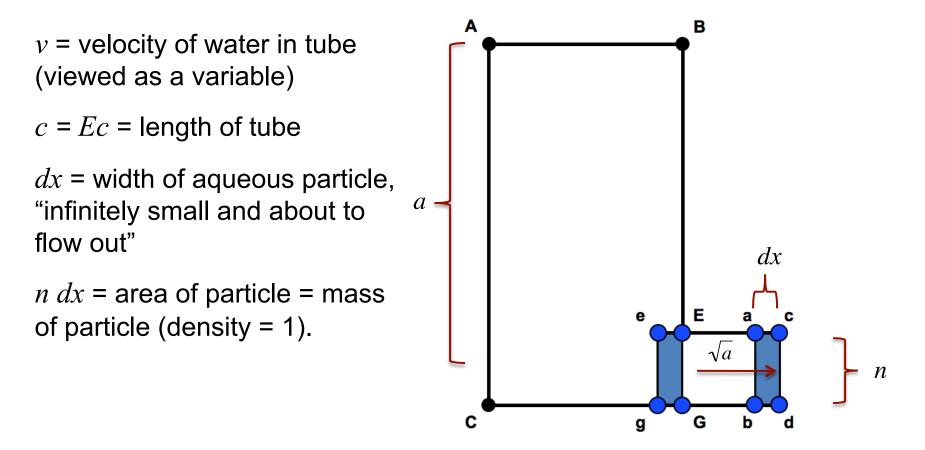
n =ratio of FD to o (FD is n times the width of the hole)

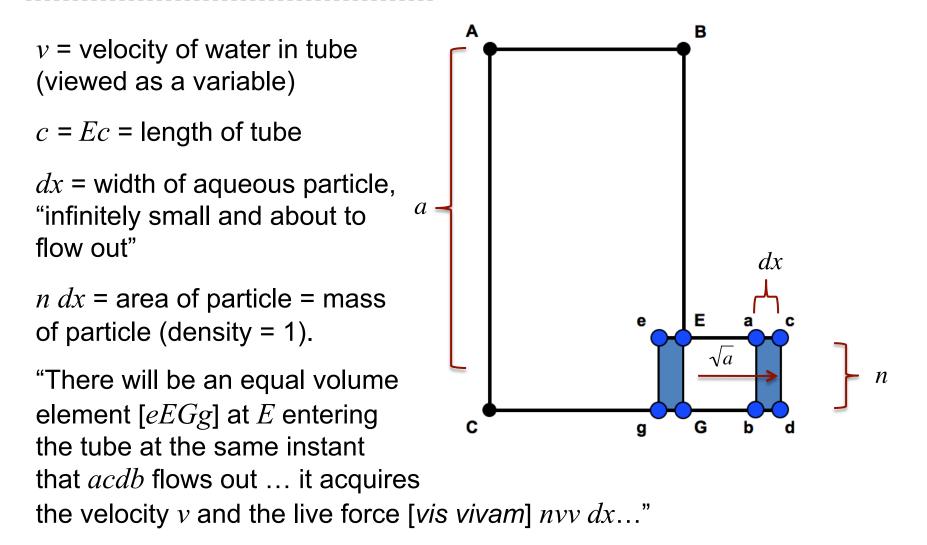
Aqueous particles at acbd (midway through tube) and eEGg (about to enter tube).

Velocity of water in tube is \sqrt{a}/n .



If tube is broken at cd, velocity of water in tube increases to \sqrt{a} .





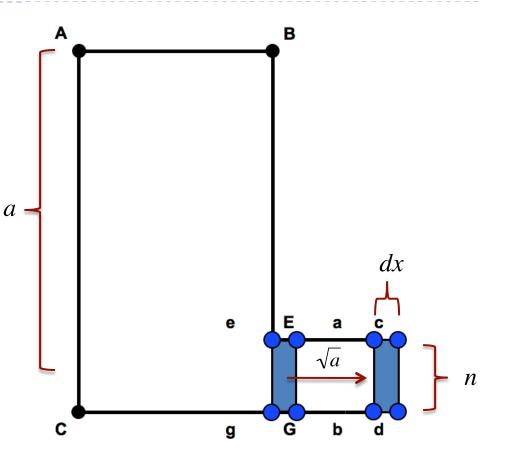
"...to this ... is to be added the increment of live force [2ncv dv] which the water at *Eb* receives while the volume element at *ad* flows out..."

Live forces (*vis viva*):

Potential ascent:

- Inflow: $(n dx)v^2$
- Outflow: 2ncv dv

Actual descent: (*n* dx)a



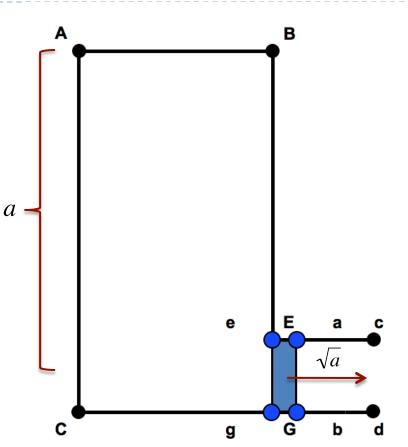
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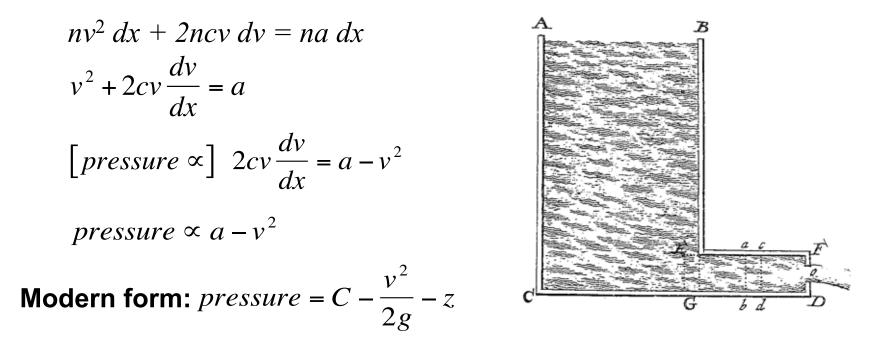
Equate potential ascent & actual descent:

 $nv^2 dx + 2ncv dv = na dx$

Modernizing Bernoulli's Conclusion

$nv^2 dx + 2ncv dv = na dx$

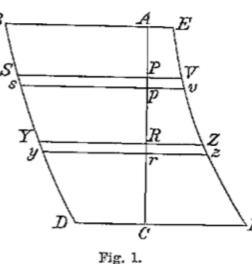
This is (almost) the Bernoulli equation for fluid flow:



A letter from Euler to Johann Bernoulli, 16 May 1739:

Sit igitur [Fig. 1] vas cujuscunque figurae A B D C, initio, quo aqua per foramen CD effluere incipit, usque ad A B aqua repletum, cujus

altitudo AC sit = a, et foraminis CDamplitudo = n. Ponamus aquam jam usque in PS subsedisse hocque tempore aquam per foramen CD effluere celeritate altitudini z debita, minimo autem tempusculo subsidere superficiem PS per spatiolum Pp; sitque Pp = dp atque amplitudo vasis PS = s, denotabit z + dzaltitudinem celeritati aquae effluentis debitam, cum suprema aquae superficies usque in ps subsedit. Ut nunc mutatio motus hoc tempusculo genita innotescat, concipie aquae RY, ponaturque AR = r, et amplitud hujus strati RY debita altitudini $\frac{nnz}{r}$; et quia







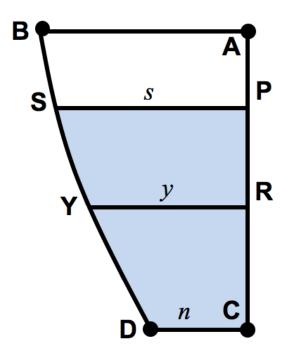
motus hoc tempusculo genita innotescat, concipiatur superficies quaecunque aquae R Y, ponaturque A R = r, et amplitudo R Y = y; erit celeritas hujus strati R Y debita altitudini $\frac{n n z}{y y}$; et quia tempusculo infinite parvo superficies R Y descendit in ry, erit tum ejus celeritas debita altitudini

Initially, surface is at PS; water flows out of hole at CD.

• z = velocity head at $PS [= V^2/2g]$

D

• (nn/yy)z = velocity head at RY [=h]

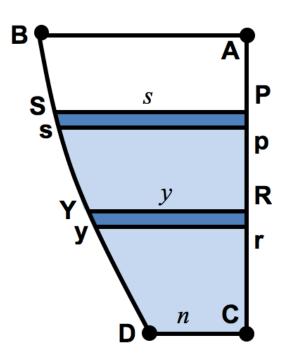


Initially, surface is at PS; water flows out of hole at CD.

- z = velocity head at $PS [= V^2/2g]$
- (nn/yy)z = velocity head at RY [=h]

In an infinitesimal span of time:

- *PS* sinks to *ps*
- *RY* sinks to *ry*

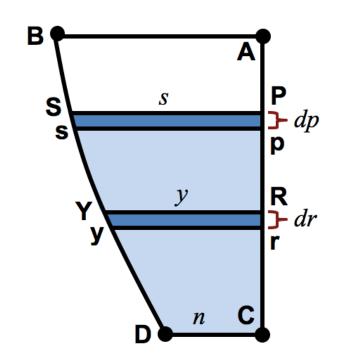


Initially, surface is at PS; water flows out of hole at CD.

- z = velocity head at $PS [= V^2/2g]$
- (nn/yy)z = velocity head at RY [=h]

In an infinitesimal span of time:

- PS sinks to ps (change = dp)
- RY sinks to ry (change = dr)
- z + dz = velocity head at ps
- Velocity head at ry= $nn/(y+dy)^2 (z+dz) [= h + dh]$

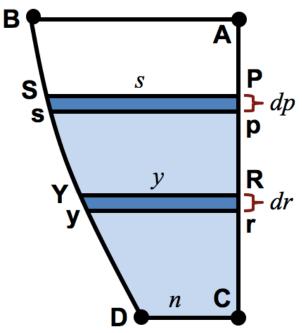


Change in velocity head from RY to $ry = (nn/yy) dz - 2nnz dy/y^3$. [= dh]

Modernizing Euler's Conclusion

Fluid density is taken to = 1; velocity head measured as square of velocity (imagine velocity units are m/s):

 $dh \ (m^2/s^2)$ $dh/dr \ (m/s^2)$ "accelerating force" $dh/dr \cdot y \ dr \ (kg \cdot m/s^2)$ "moving force" $dh/dr \cdot y \ dr/y = dh \ (N/m)$ [pressure dp]



Modernizing Euler's Conclusion

Fluid density is taken to = 1; velocity head measured as square of velocity (imagine velocity units are m/s):

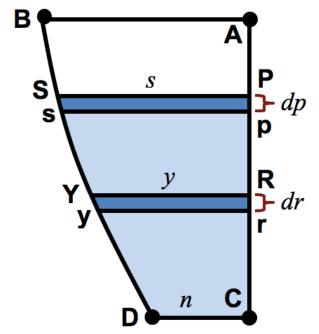
 $dh \ (m^2/s^2)$ $dh/dr \ (m/s^2) \ \text{``accelerating force''}$ $dh/dr \ \cdot y \ dr \ (kg \cdot m/s^2) \ \text{``moving force''}$ $dh/dr \ \cdot y \ dr/y = dh \ (N/m) \ [\text{ pressure } dp \]$

Euler thus obtains pressure differential:

 $[dp] = (nn/yy)dz - 2nnz dy/y^3.$

Then he uses 1/y = dr/(s dp) to get

$$[dp] = nn[dz/(s dp) \cdot dr/y - 2z dy/y^3]$$



Modern integration yields: $p(y) - p(s) = \frac{n^2 dz}{s dp} \int_s^y \frac{dr}{y} + \frac{n^2}{s^2} z - \frac{n^2}{y^2} z$



Euler's Fluid Mechanics Papers



E332 Written 1751 Published 1767

E258 Written 1752 Published 1761

E226 Written 1755 Published 1757

D

PRINCIPES GÉNÉRAUX DU MOUVEMENT DES FLUIDES.

MOTVS FLVIDORVM.

Euler's Fluid Mechanics Papers

LE

E332 Written 1751 Published 1767

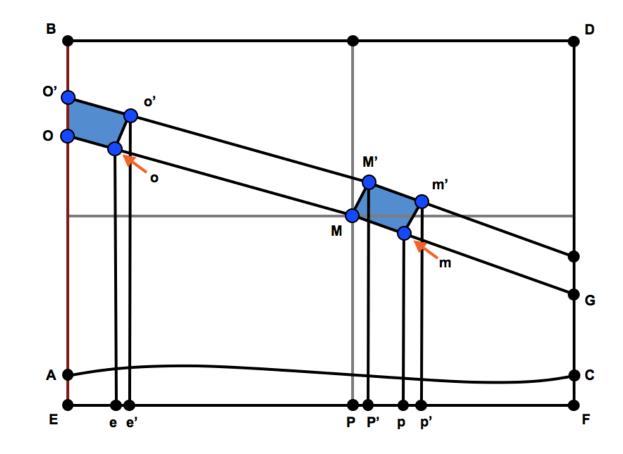
RECHERCHES sur mouvement des rivieres.

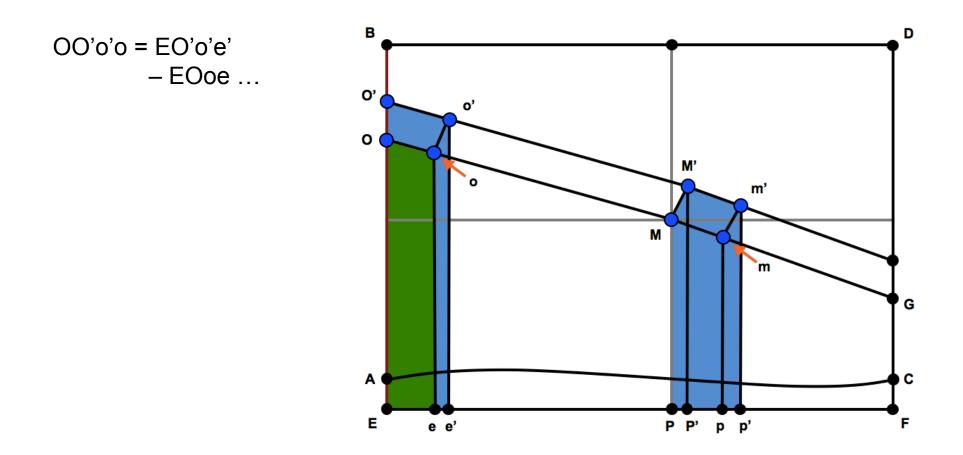
§. 5. Soit donc AC le lit d'une telle fection de riviere, ou Fig. 1. d'une riviere infiniment étroite, qui ait partout la même largeur infiniment petite. Que ce lit AC foit une ligne courbe quelconque, qui est fupposée être connue; pour cet effet je conçois une ligne horizontale EF qui ferve d'axe pour y rapporter la ligne AC par des coordonnées orthogonales EP & PQ. Que ABCD foit la riviere, qui se meut sur ce lit AC, & BD sa superficie supreme; de plus je supposée, que la riviere se trouve déjà dans un état permanent ou d'équilibre, de forte que sa superficie BD demeure continuellement la même, & qu'aux mêmes points, comme M, les particules d'eau qui y passent toujours les mêmes vites, & qu'elles soient assure assures aux mêmes pressions.

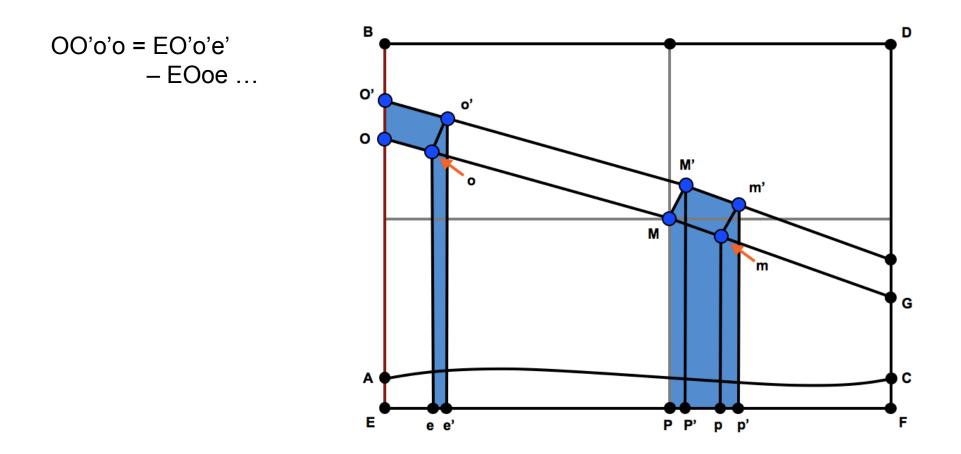
Water in the river has constant density = 1.

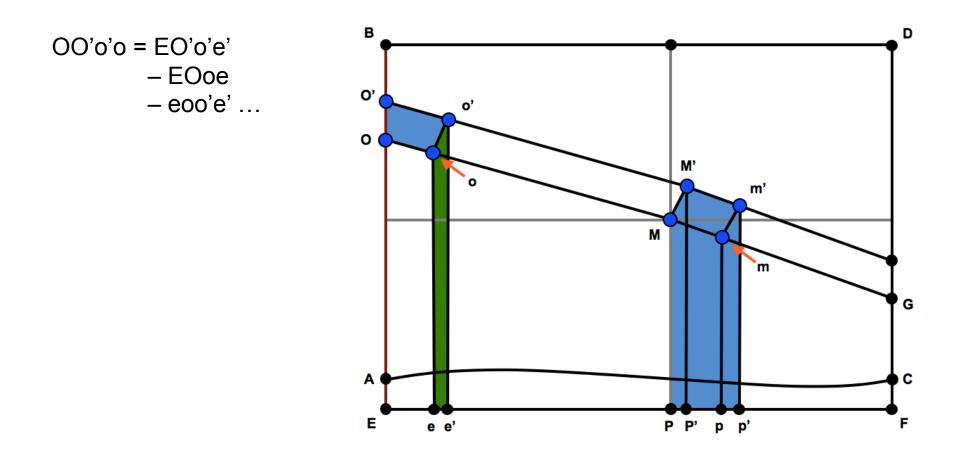
Fluid particle flows downstream from left (OO'o'o) to right (MM'm'm).

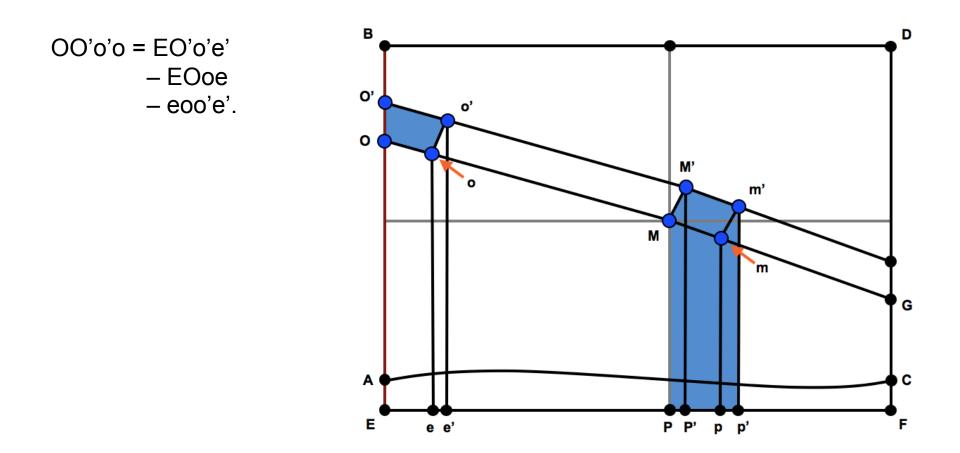
Since the fluid is *incompressible*, the area of OO'o'o must equal the area of MM'm'm.

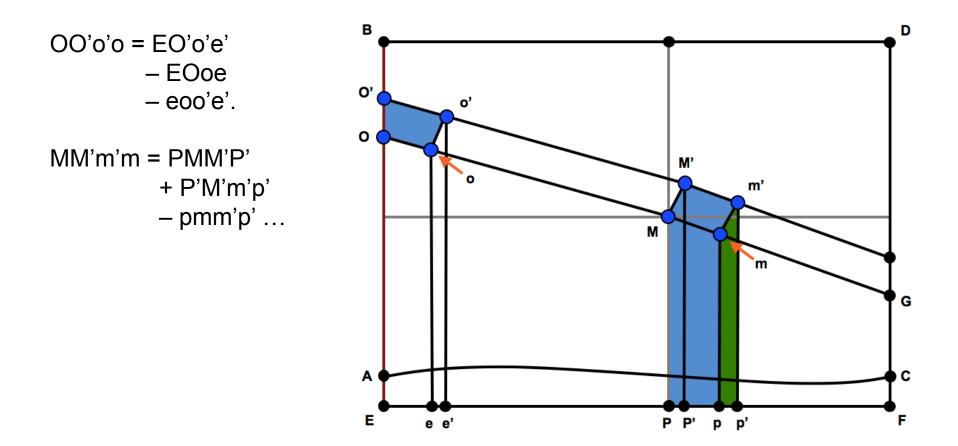


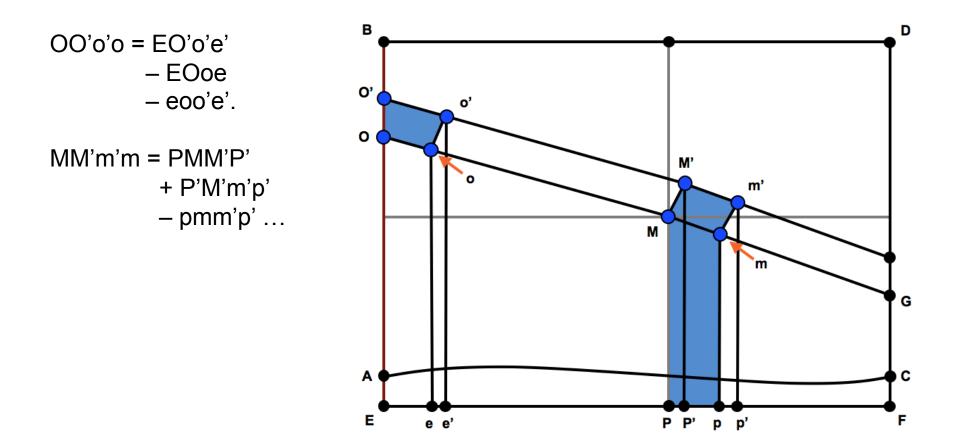


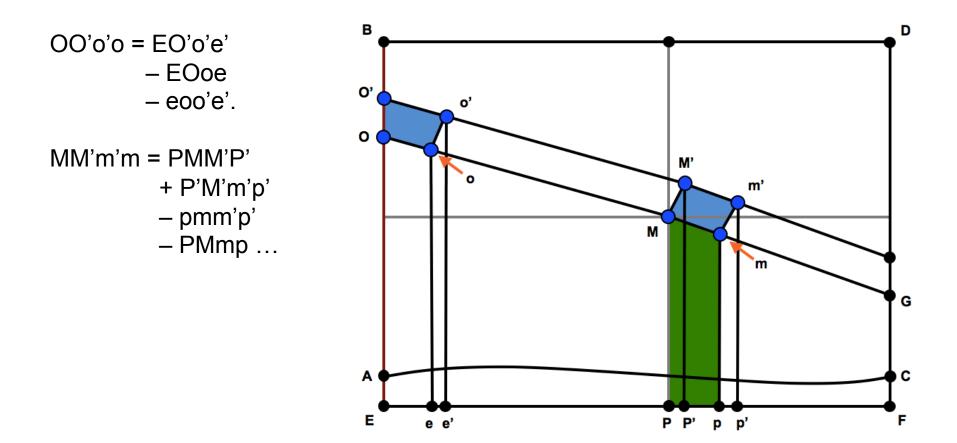


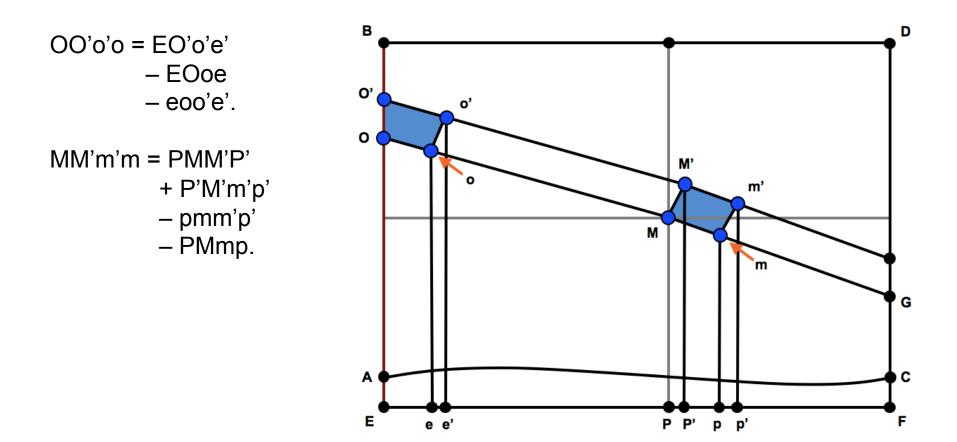




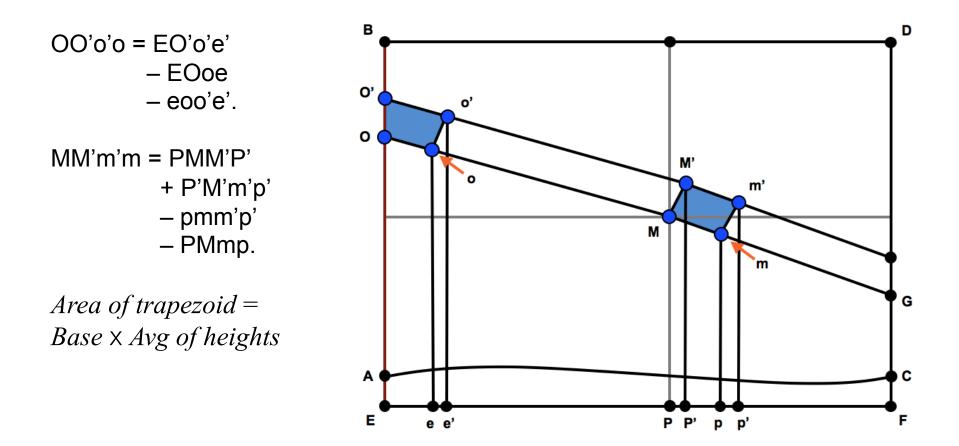


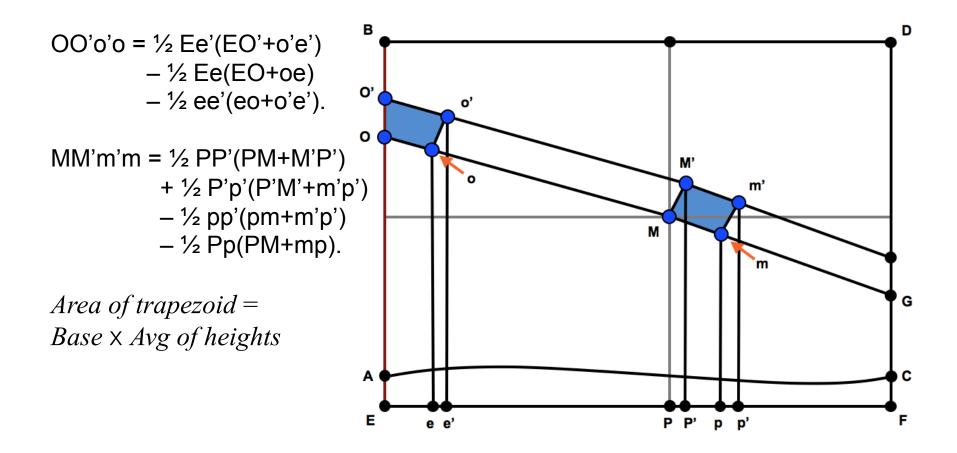






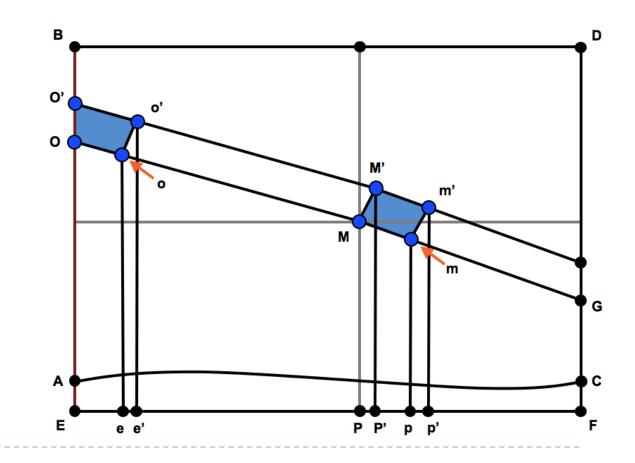
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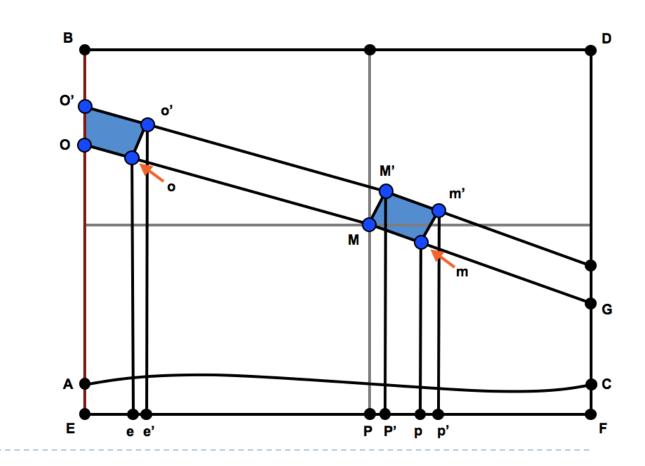
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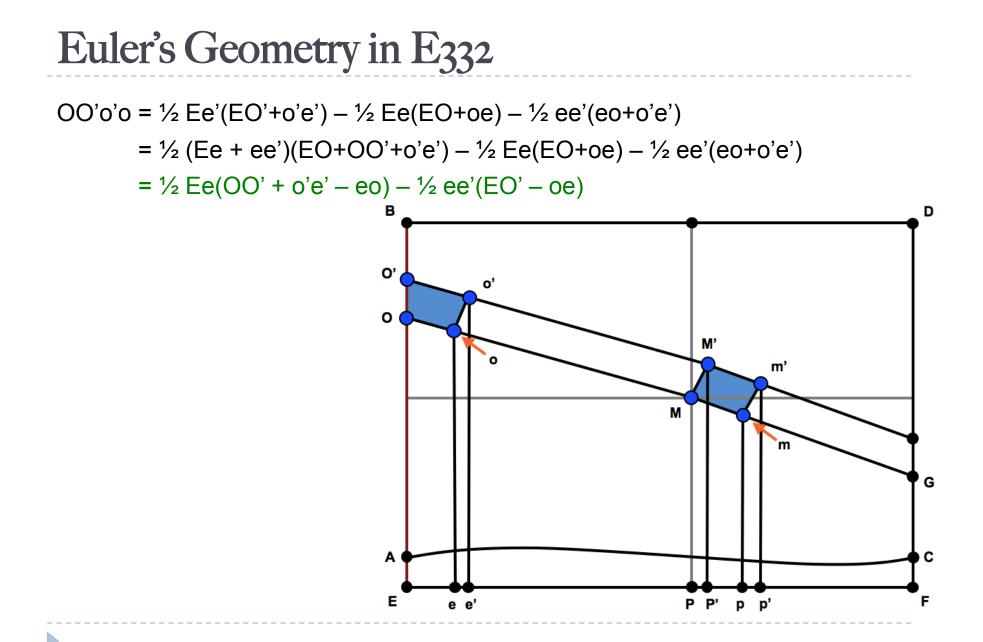
OO'o'o = ¹/₂ Ee'(EO'+o'e') - ¹/₂ Ee(EO+oe) - ¹/₂ ee'(eo+o'e')



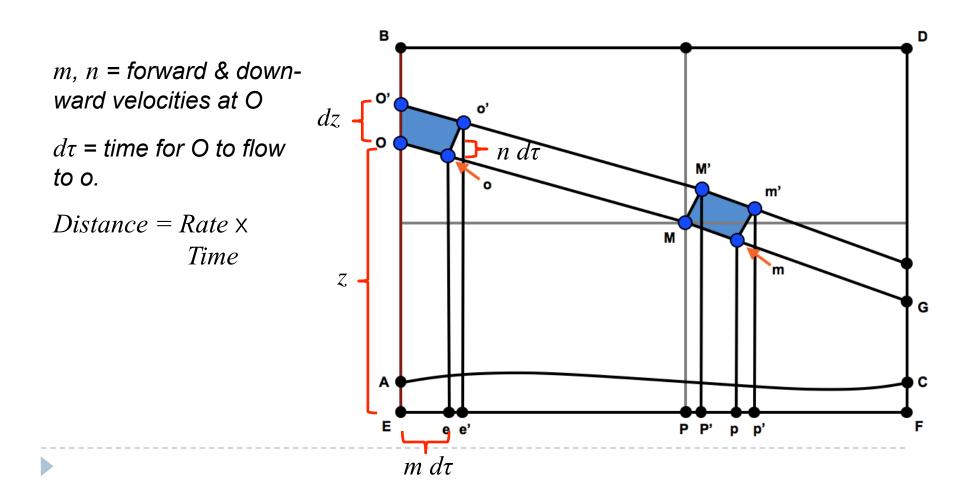
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$OO'o'o = \frac{1}{2} Ee'(EO'+o'e') - \frac{1}{2} Ee(EO+oe) - \frac{1}{2} ee'(eo+o'e')$ = $\frac{1}{2} (Ee + ee')(EO+OO'+o'e') - \frac{1}{2} Ee(EO+oe) - \frac{1}{2} ee'(eo+o'e')$

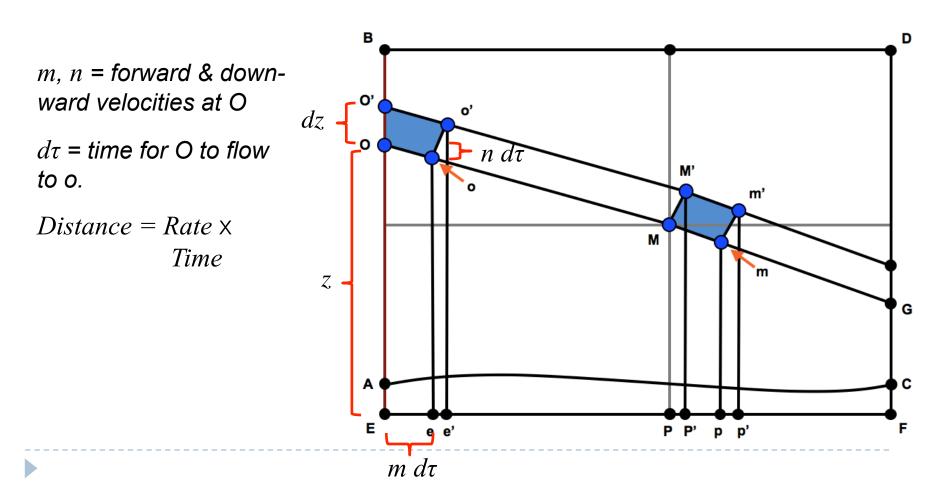


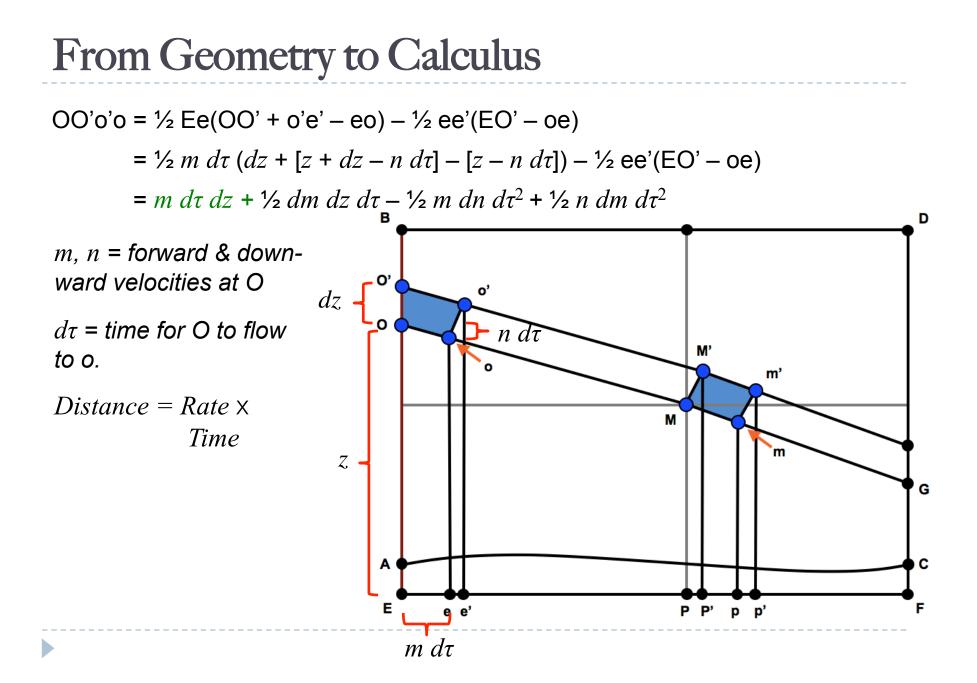


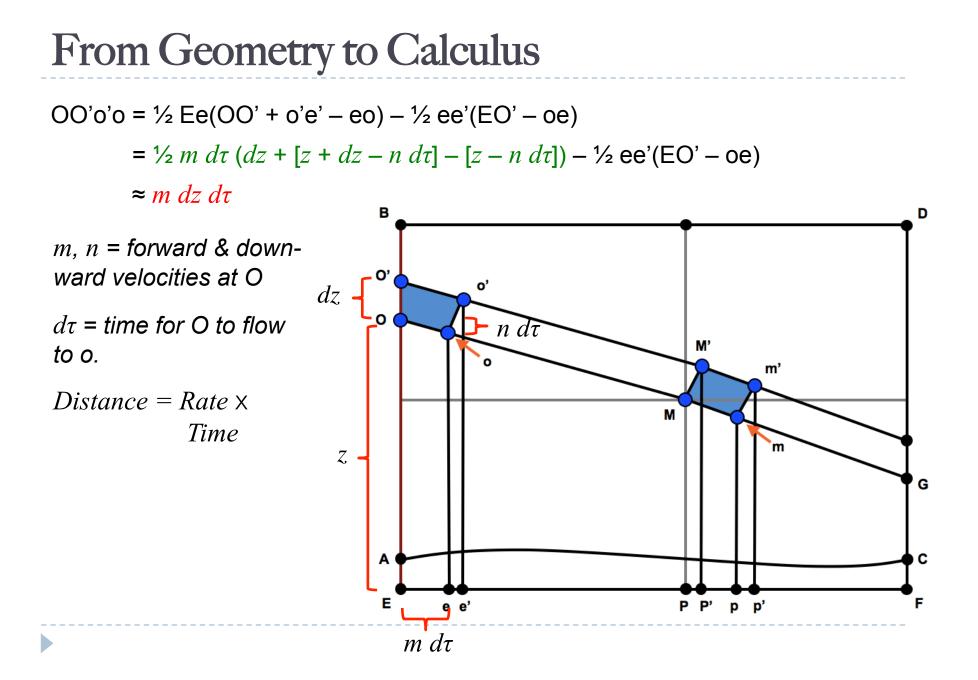
 $OO'o'o = \frac{1}{2} Ee(OO' + o'e' - eo) - \frac{1}{2} ee'(EO' - oe)$



OO'o'o = $\frac{1}{2}$ Ee(OO' + o'e' - eo) - $\frac{1}{2}$ ee'(EO' - oe) = $\frac{1}{2}m d\tau (dz + [z + dz - n d\tau] - [z - n d\tau]) - \frac{1}{2}$ ee'(EO' - oe)



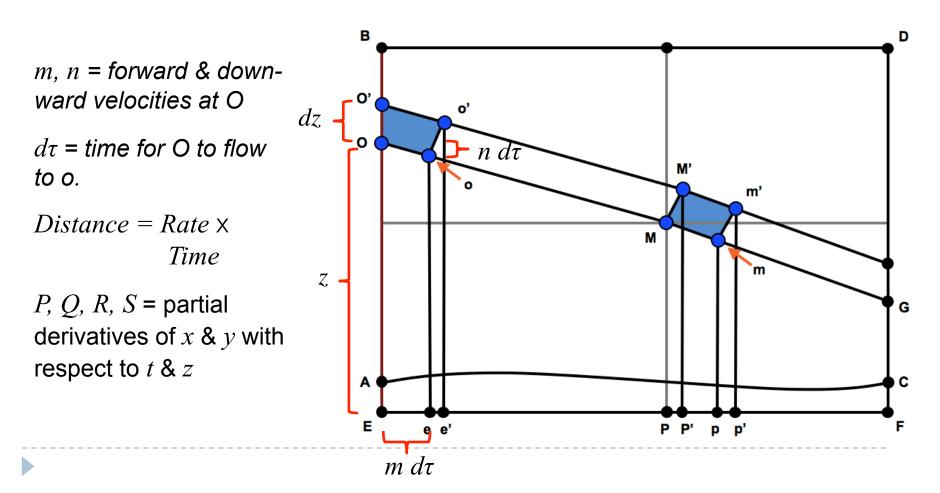




From Geometry to Calculus

OO'o'o $\approx m dz d\tau$

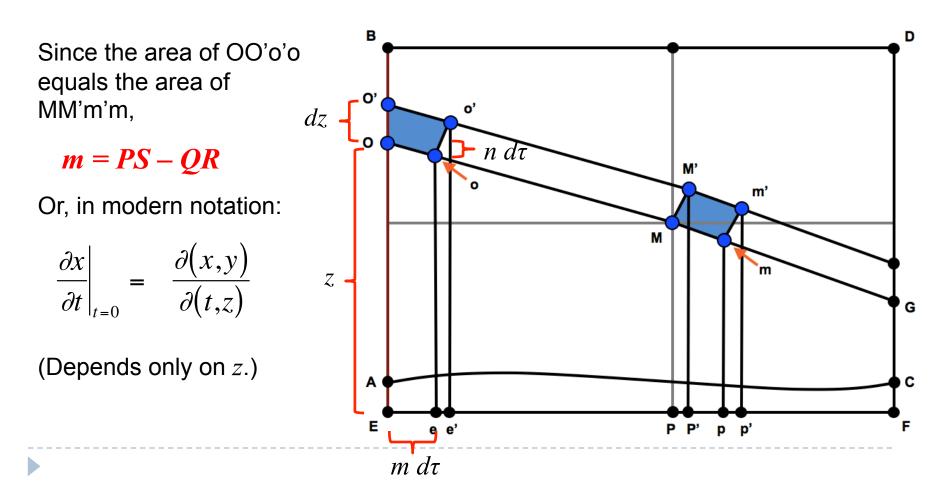
MM'm'm $\approx PS dz d\tau - QR dz d\tau = (PS - QR) dz d\tau$

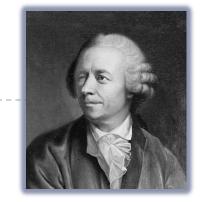


From Geometry to Calculus

OO'o'o $\approx m dz d\tau$

MM'm'm $\approx PS dz d\tau - QR dz d\tau = (PS - QR) dz d\tau$





Euler's Fluid Mechanics Papers

RECHERCHES sur le mouvement des rivieres.

E332 Written 1751 Published 1767

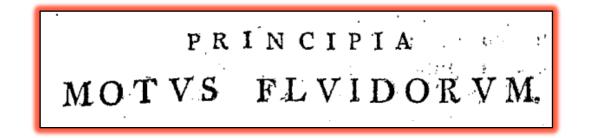
> PRINCIPIA MOTVS FLVIDORVM.

E258 Written 1752 Published 1761

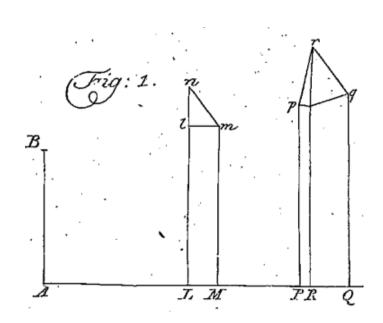
E226 Written 1755 Published 1757

PRINCIPES GÉNÉRAUX DU MOUVEMENT DES FLUIDES.

E258 Written 1752 Published 1761



13. Cum igitur fit du = L dx + I dy et dy = M dx + m dy, hinc geminas celeritates cuiusque alius puncti, quod quidem infinite parum a puncto l diffat, affignare heebit; fi enim talis puncti a puncto l diffantia fecundum axem AL fit = dx, et fecundum axem AB = dy, tum huius puncti celeritas fecundum axem AL erit = u + L dx + l dy; celeritas autem fecundum alterum axem AB = v + M dx + m dy. Tempulculo ergo infinite paruo dt hoc punctum proferetur fecundum directionem axis AL per spatiolum = dt (u + L dx) + l dy et secundum directionem alterius axis AB per spatiolum = dt(v + M dx + m dy).

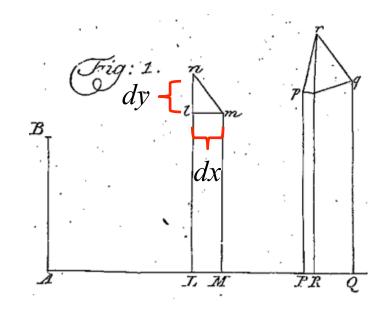


Fluid triangle ℓ mn flows to fluid triangle pqr in infinitesimal time dt.

$$u = dx = \ell m$$

$$v = dy = \ell n$$

fit $L + m \equiv 0$. Seu cum fit $L \equiv \frac{du}{dx}$ et $m \equiv \frac{dv}{dy}$, celeritates u et v, quae puncto l fecundum directiones axium AL et AB ineffe concipiuntur, eiusmodi functiones coordinatarum x et y effe debent, vt fit $\frac{du}{dx} + \frac{dv}{dy} \equiv 0$, ficque motuum poffibilium criterium in hoc confiftit, vt fit $\frac{du}{dx} + \frac{dv}{dy} \equiv 0$; nifi enim hacc condi-



Fluid triangle ℓ mn flows to fluid triangle pqr in infinitesimal time dt.

 $u = dx = \ell m$ $v = dy = \ell n$

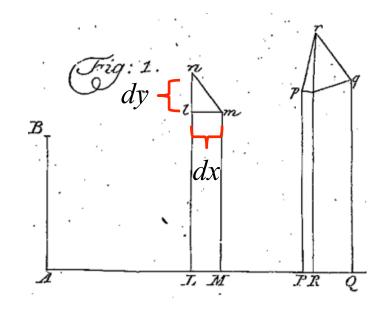
 $L = du/dx, \quad \ell = du/dy$ $M = dv/dx, \quad m = dv/dy$

 $du = L \, dx + \ell \, dy, \quad dv = M \, dx + m \, dy$

Argument similar to E332 shows that

L+m=0.

fit $L + m \equiv 0$. Seu cum fit $L \equiv \frac{du}{dx}$ et $m \equiv \frac{dv}{dy}$, celeritates u et v, quae puncto l fecundum directiones axium AL et AB ineffe concipiuntur, eiusmodi functiones coordinatarum x et y effe debent, vt fit $\frac{du}{dx} + \frac{dv}{dy} \equiv 0$, ficque motuum poffibilium criterium in hoc confiftit, vt fit $\frac{du}{dx} + \frac{dv}{dy} \equiv 0$, nifi enim hacc condi-



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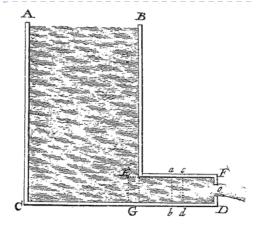
PRINCIPES GÉNÉRAUX DU MOUVEMENT DES FLUIDES.

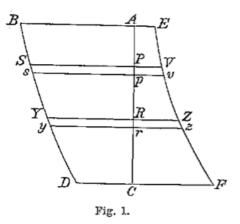
niment peu incliné à l'axe OC. Donc, fi nous confidérons un paralielepipede rectangle ZPQRzpqr formé des trois côtés $ZP \equiv dx$, $ZQ \equiv dy$, & $ZR \equiv dz$, le fluide qui occupoit cet espace fera transporté pendant le tems dt à remplir l'espace Z/P'Q'R'z'p'q'r', infiniment peu différent d'un parallelepipede rectangle, dont les trois côtés feront :



Cubical fluid particles, 3 dimensions; techniques are more algebraic.

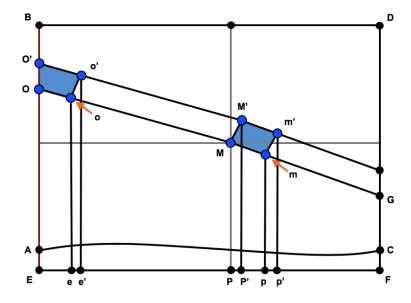
1738-39 – D. Bernoulli & Euler use method of parallel sections. Bernoulli argues using actual descent & potential ascent; Euler uses "moving forces".





1738-39 – D. Bernoulli & Euler use method of parallel sections. Bernoulli argues using actual descent & potential ascent; Euler uses "moving forces".

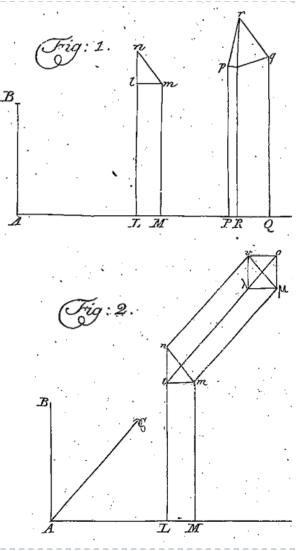
1751 – Euler uses quadrilateral fluid particle method, derives formulas with Euclidean geometry in 2D. Awkward notation involving initial conditions.



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1752 – Euler uses triangular & tetrahedral fluid particles, and same Euclidean techniques. Begins to use consistent notation for partial derivatives.

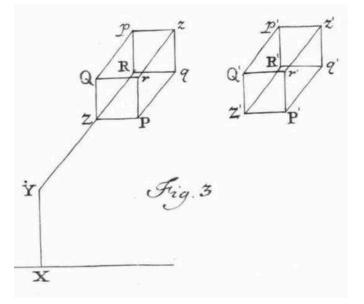


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1752 – Euler uses triangular & tetrahedral fluid particles, and same Euclidean techniques. Begins to use consistent notation for partial derivatives.

1755 – Euler uses cubical fluid particles. Less geometric than previous two works.



Epilogue – Lagrange's *Mécanique Analytique* (1788)

Some Conclusions:

- Serious notational deficiencies; key concepts still in development
- Potential ascent & actual descent eventually replaced by modern notion of force.
- Earlier: geometry drives the algebraic argument
- Later: algebra and analysis dominate, geometry reduced to more of an illustration
- Euler's work in 1739-1755 followed this pattern, becoming more flexible and less dependent on geometry.

D

Nous supposerons que le fluide soit homogène & pesant, & qu'il parte du repos, ou qu'il soit mis en mouvement par l'impulsion d'un piston appliqué à sa surface; ainsi les vîtesses p, q, r, de chaque particule, devront être telles que la quantité p dx + q dy + r dz soit intégrable (art. 18); par conséquent on pourra employer les formules de l'article 20.

Soit donc φ une fonction de x, y, $z \ll t$, déterminée par l'équation

$$\frac{d^{1}\phi}{dx^{2}} + \frac{d^{1}\phi}{dy^{2}} + \frac{d^{2}\phi}{dz^{2}} = 0$$

on aura d'abord pour les vîtesses de chaque particule, suivant les directions des coordonnées x, y, z, ces expressions,

$$p = \frac{d\phi}{dx}, \ q = \frac{d\phi}{dy}, \ r = \frac{d\phi}{dz}.$$

Enfuite on aura

$$\lambda = V + \frac{d\phi}{dz} + \frac{1}{2} \left(\frac{d\phi}{dz} \right)^2 + \frac{1}{2} \left(\frac{d\phi}{dy} \right)^2 + \frac{1}{2} \left(\frac{d\phi}{dz} \right)^2,$$

quantité qui devra être nulle à la furface extérieure libre du fluide (art. 2).

Geometry vs. Analysis

"The analytical investigations of the Greek geometers are indeed models of simplicity, clearness and unrivalled elegance... some of the noblest monuments of human genius. It is a matter of deep regret, that Algebra, or the Modern Analysis, from the mechanical facility of its operations, has contributed, especially on the Continent, to vitiate the taste and destroy the proper relish for the strictness and purity so conspicuous in the ancient method of demonstration."

— John Leslie, preface to *Elements of Geometry* (1809)^[9]



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Geometry vs. Analysis

"... the basic physico-mathematical tools of the modern derivation of Euler's equations were not originally available. In the early eighteenth century there was no concept of a dimensional quantity, no practice of writing vector equations (even in the so-called Cartesian form), no concept of a velocity field, and no calculus of partial differential equations. The idea of founding a domain of physics on a system of general equations rather than on a system of general principles expressed in words did not exist."

— Oliver Darrigol, introduction to Worlds of Flow (2005)^[2]

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References

- [1] Bernoulli, Daniel. *Hydrodynamica*. Basel: Dulsecker, 1738. (English Translation by T. Carmody and H. Kobus, Dover, 1968.)
- [2] Darrigol, Oliver. *Worlds of Flow: A History of Hydrodynamics From the Bernoullis to Prandtl.* New York: Oxford University Press, 2005.
- [3] Euler, Leonhard. "Recherches sur le mouvement des rivières". *Mémoires de l'académie des sciences de Berlin* **16** (1767), pp. 101-118. Numbered E332 in Eneström's index. Available at eulerarchive.maa.org.
- [4] —. "Principia motus fluidorum". Novi commentarii academiae scientiarum Petropolitanae, 6 (1756/7)
 1761, pp. 24-26, 271-311. Numbered E258 in Eneström's index. Available at http://eulerarchive.maa.org.
- [5] —. "Principes generaux du mouvement des fluides". Mémoires de l'académie des sciences de Berlin 11 (1755), 1757, pp. 274-315. Numbered E226 in Eneström's index. Available at http://eulerarchive.maa.org.
- [6] —. Letter to Johann Bernoulli, 16 May 1739. Published in *Bibl. Math* 63 (1905), pp. 24-33. Numbered E863 in Eneström's index. Available at <u>http://eulerarchive.maa.org</u>.
- [7] Lagrange, Joseph Louis. Traité de méchanique analytique. Paris: Desaint, 1788.
- [8] Mikhailov, Gleb. Introduction to Die Werke von Daniel Bernoulli, Vol. 5. Basel: Birkhäuser, 2002.
- [9] Timmons, Todd. Mathematics in Nineteenth Century America: The Bowditch Generation. Chestnut Hill, MA: Docent Press, 2013.
- [10] Truesdell, Clifford. "Rational Fluid Mechanics, 1657–1765." In Euleri Opera Omnia, Ser. 2, Vol. 12. Lausanne: Orell Füssli Turici, 1964. pp. IX–CXXV.

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